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RESEARCH MEMORANDUM

PRESSURES AND ASSOCIATED AERODYNAMIC AND LOAD

CHARACTERISTICS FOR TWO BODIES OF

REVOLUTION AT TRANSONIC SPEEDS

By Harold L. Robinson

Langley Aeronautical Laboratory
Langley Field, Va.

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PRESSURES AND ASSOCIATED AERODYNAMIC AND LOAD

CHARACTERISTICS FOR TWO BODIES OF

REVOLUTION AT TRANSONIC SPEEDS

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SUMMARY

Analysis of the results obtained from a transonic wind-tunnel investigation of two bodies of revolution having the same nose shape, one incorporating a cylindrical afterbody and the other incorporating a curved afterbody, indicated that the pressures over the forward portions of the bodies were the same, whereas, the induced velocities over the rearward portions of the curved body were greater than those over the cylindrical body. However, the cross-section normal loads were greater over the rearward portions of the cylindrical body. Variation of the aerodynamic characteristics with Mach number was rather small for both bodies. The cylindrical body exhibits better stability characteristics than the curved body. The theory of NACA Rep. 1048 regarding the aerodynamic characteristics of the bodies is in fair agreement with the results of this paper.

INTRODUCTION

A detailed study of the pressures and resulting forces for a body of revolution, designated "curved body" in this report, at transonic speeds has been presented in reference 1.

The present tests were undertaken in order to provide aerodynamic load data for a body of revolution having an ogive nose and cylindrical afterbody and to compare the aerodynamic characteristics of this body with the body of reference 1 at transonic speeds. The body used in the present test is designated "cylindrical body" herein. A comparison of various theoretical aerodynamic parameters with experimental values is included.

The tests reported herein were made for a Mach number range from 0.6 to 1.13 and an angle-of-attack range from 0° to 20°. The Reynolds number

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range corresponding to the Mach number range varied from 3.3×10^6 to 3.9×10^6 per foot of length.

SYMBOLS

A_p	plan-form area of body
C_{M_F}	pitching-moment coefficient around the nose, based on maximum body cross-sectional area and body length
C_{N_F}	normal-force coefficient, based on maximum body cross-sectional area
c_{d_c}	section drag coefficient of an infinite cylinder
c_n	transverse section normal-force coefficient, $\dfrac{N_t}{qD\,d(x)}$
c_{nn}	meridian load coefficient, $\dfrac{N_n}{qLR_{max}\,d(\theta)}$
D	diameter of body at any station
L	length of body
M	Mach number
N_n	elemental force on meridian body section of width $R\,d(\theta)$ (force vector is normal to body axis and makes an angle θ with vertical plane of symmetry)
N_t	elemental force on transverse body section of length $d(x)$ (force vector is normal to horizontal plane of symmetry)
P	pressure coefficient
Q	volume of body
q	dynamic pressure
R	radius of body at any station
S_b	base area of body

x   distance from nose of model, positive rearward

x_m moment center

x_p centroid of body plan-form area

x_{cp} center-of-pressure location

y   distance from vertical plane of symmetry

α angle of attack

η ratio of the drag coefficient of a finite cylinder to the
                section drag coefficient of an infinite cylinder at
                $\alpha = 90^{\circ}$

θ meridian station, 0° at top

Subscripts:

max   maximum value

L   lower surface

U   upper surface

APPARATUS AND METHODS

Tunnel

All the data discussed herein were obtained from tests conducted in
the Langley 8-foot transonic tunnel. At present, this tunnel has a
dodecagonal slotted test section and is capable of continuously variable
operation through the speed range up to a Mach number of 1.14. A test
section used previously in this tunnel did not incorporate slots, but
had a closed throat. All the data for the cylindrical body and most of
the data for the curved body were obtained from tests in the slotted test
section. A small portion of the data for the curved body was obtained
from tests in the closed-throat test section.

Tunnel-wall-interference corrections were not applied to the data
obtained from tests in the slotted test section because choking and
blockage effects are negligible, especially for the small ratio of model
to tunnel size of the present tests. Effects of wall-reflected disturb-
ances have been reduced by offsetting the model from the tunnel center
line.

Bodies

A drawing of the two bodies is presented in figure 1. The cylindrical body has the same dimensions as body D of reference 2. The curved body is the same body as that used in references 1 and 3 and is similar to, but slightly longer than, body A of reference 2. Both the curved and cylindrical bodies have the same dimensions forward of the 20-inch body station.

Each of the models was instrumented with six rows of orifices spaced along meridians of the body. Each row contained 20 or more orifices. The relative size of the stings employed to support the model in the tunnel is indicated in figure 1.

Measurements

Pressure.- The pressures existing on the surface of the cylindrical body were measured by connecting the orifices to a multitubed manometer. In order to determine the forces on the model, these pressures were integrated as discussed in the section of this report entitled "Presentation of Results." The pressure data and associated aerodynamic parameters for the curved body were obtained from references 1 and 3.

The repeatability of the pressure data presented herein as affected by the pressure measurements, angle of attack, orifice size and location, and other factors may be judged from figure 2. The largest errors occur near the nose where they are as large as $\Delta P = \pm 0.015$. The accuracy is much better over the remainder of the body. The average error, as determined from the data presented in figure 2, is $\Delta P = \pm 0.005$.

Angle of attack.- The angle of attack for the cylindrical body was measured by an electrical strain-gage pendulum device mounted internally near the base of the support sting. Sting and model deflections occurring ahead of this point, due to forces and moments acting on the model, were determined from static tests. These corrections were applied to the angles of attack, although the maximum deflections occurring during the investigation were approximately 0.1°. The angles of attack were also corrected for the approximately 0.1° upflow existing in the Langley 8-foot transonic tunnel. The absolute accuracy of the angle-of-attack measurements is estimated to be within 0.1°.

PRESENTATION OF RESULTS

Pressure Coefficients

All the pressures measured for the cylindrical body are presented in table 1. The longitudinal distribution of pressure coefficients for the cylindrical body at 0° angle of attack is presented in figure 3. Also shown in this figure is the pressure distribution for the curved body from references 1 and 3. The longitudinal distribution of pressure coefficient at the other angles of attack are presented in figure 4 at three Mach numbers (approximately 0.8, 1.00, and 1.13).

Normal Force and Pitching Moment

A comparison of the normal-force and pitching-moment coefficients for the two bodies is presented in figures 5 and 6, respectively. All the data for the curved body were obtained from reference 1. In order to compare the pitching-moment characteristics of the two bodies, the moment coefficients were taken about the nose of the bodies.

The integral equation used to compute the normal-force coefficients for the cylindrical body was

$$C_{N_F} = -\frac{8L}{D_{max}} \int_0^{0.5} \cos\theta \left[\int_0^1 P \frac{D}{D_{max}} d\left(\frac{x}{L}\right) \right] d\left(\frac{\theta}{2\pi}\right)$$

and that used to compute the pitching-moment coefficient was

$$C_{M_F} = \frac{8L}{D_{max}} \int_0^{0.5} \cos\theta \left[\int_0^1 P \frac{D}{D_{max}}\left(\frac{x}{L}\right) d\left(\frac{x}{L}\right) \right] d\left(\frac{\theta}{2\pi}\right)$$

The coefficients presented at $\alpha = 20°$ could have been lowered as much as 25 percent of the value shown by changing the fairings of the graphical integrations. However, the data presented for the cylindrical body agree with the strain-gage data presented in reference 2. The fairing choice does not exist at $\alpha \leq 8°$ but this margin increases with angle of attack as the angle is increased from 8°.

The theoretical values of normal-force and pitching-moment coefficient shown in figures 5 and 6 were computed by the method described in reference 4. The equations for these coefficients may be written as follows:

$$C_{N_F} = \frac{8S_b}{\pi D_{max}^2} \alpha + 4\eta c_{d_c} \frac{A_p}{\pi D_{max}^2} \alpha^2$$

$$C_{M_F} = \frac{8}{\pi D_{max}^2}\left(\frac{Q}{L} - S_b\right) \alpha - 4\eta c_{d_c} \frac{A_p}{\pi D_{max}^2}\left(\frac{x_p}{L}\right) \alpha^2$$

The values of η and c_{d_c} used in the calculations for the cylindrical body were 0.7 and 1.2 and were chosen from reference 5 and references 6 and 7, respectively. The plan-form area A_p, the body volume Q, and the location of the centroid of the body plan-form area x_p were determined from graphical integrations of suitable geometric parameters.

Center of Pressure

A comparison of the center-of-pressure locations for the two bodies is presented in figure 7. The data for the cylindrical body were computed from the normal-force and pitching-moment coefficients of figures 5 and 6. The center-of-pressure data for the curved body were obtained from reference 1.

Detailed Aerodynamic Loads

The meridian normal-load distribution is presented for three Mach numbers (0.80, 1.00, and 1.13) through the angle-of-attack range in figure 8. This coefficient c_{nn} is defined in such a manner that the load perpendicular to the fuselage center line on a stringer section $Rd(\theta)$ wide is $c_{nn}qlR_{max} d(\theta)$. Accordingly, c_{nn} is computed from the graphical integration along a body meridian as follows:

$$c_{nn} = -\int_0^1 \frac{D}{D_{max}} P\, d\left(\frac{x}{L}\right)$$

The longitudinal distribution of body cross-section normal loads at $M = 1.00$ is presented in figure 9. The pressure data were computed by a graphical integration

$$c_n = \int_0^1 \left(P_L - P_U\right) d\left(\frac{y}{R}\right)$$

The theoretical values of $c_n \dfrac{D}{D_{max}}$ were computed by the method of reference 4. The equation for a body of revolution may be written as follows:

$$c_n = \pi \left(\frac{dD}{dx}\right) \alpha + \eta c_{d_c} \alpha^2$$

DISCUSSION OF RESULTS

Pressure Distribution

The pressures over the nose of both bodies, forward of the 20-inch station, are very similar to each other through the range investigated (figs. 3 and 4). Some of the differences observed near the tip of the nose are due to slight differences in the body shape at the apex. In general, the pressures over the rearward portions of the curved body are lower than those over the rearward portions of the cylindrical body. The typically characteristic rearward movement of the shock location with Mach number increases may be observed in figure 3. At $M = 0.99$ the shock is located at approximately the 20-inch body station of the cylindrical body, whereas at $M = 1.03$ the shock has moved to the 37-inch body station.

The compressions shown for the cylindrical body in figure 3 at $M = 1.08$ and 1.10 at approximately the 30- and 34-inch stations, respectively, are probably due to the bow wave reflected from the tunnel wall and would not be evidenced in free flight. The expansions seen at the rear of the cylindrical body are caused by the air turning around the corner.

Normal-Force Characteristics

As shown in figure 5, the cylindrical body develops greater normal force at a given angle of attack and Mach number than the curved body. The change in normal-force coefficient with Mach number is insignificant at the lower angles of attack, but there is a small increase in normal-force coefficient with Mach number at the higher angles of attack.

The prediction of the normal-force coefficients by the method of reference 4 is rather accurate at the lower angles of attack. In general, the measured values fall well below the theoretical values at the higher angles of attack. As mentioned previously, alternative fairings permissible for the integrations would result in even lower values for the measured data. The cross-flow Mach number is less than 0.4 at the highest

stream Mach number and at an angle of attack of 20°. Accordingly, the values of c_{d_c} are constant. Therefore, the theory does not predict the variation of normal force with Mach number shown by the measurements.

Pitching-Moment and Center-of-Pressure Characteristics

Examination of the pitching-moment data (fig. 6) indicates that the curved body exhibits either neutral or slightly unstable characteristics for the center of gravity at the nose or unstable characteristics for more rearward locations of the center of gravity. The cylindrical body exhibited more stable characteristics inasmuch as the center of pressure is located behind the 12-inch station for all conditions. It is also noted that the variation of the center-of-pressure location with Mach number is irregular and small (fig. 7).

The agreement of the measured pitching-moment coefficient with the theory is similar to that found for the normal-force coefficients. In general, when the normal-force coefficients are overpredicted, the negative pitching-moment coefficients are also overpredicted. Examination of the equations for C_{N_F} and C_{M_F}, given in the section entitled "Presentation of Results," indicates that the probable cause for the disagreement noted between the measured and predicted coefficients is associated with the values selected for η and c_{d_c}. Had lower values of c_{d_c} and η been used the agreement would have been better.

Detailed Load Characteristics

The maximum meridian load is developed at approximately the 105° meridian (fig. 8). It is observed that the loads do not vary appreciably with Mach number.

Examination of figure 9 indicates that although the cross-section normal loads over the forward portions of both bodies are similar, the loads over the rear portion of the cylindrical body are greater than those for the curved body. This is the reason that the pitching-moment characteristics of the cylindrical body are more stable than those for the curved body. The differences observed between the normal-force and pitching-moment characteristics for the two bodies are not caused by the added length of the cylindrical body.

Comparisons of the measured and theoretical values of cross-section normal-load coefficient indicate that the theory is in fair agreement with the measured values at angles of attack below 12°. The theoretical values show the same agreement at the forward and rearward portions of the cylindrical body. It is concluded that the errors between theory

and measurement for the cylindrical body at the higher angles of attack are due to the inadequacy of available data for selecting η and c_{d_c}. The disagreement between the theory and the measurements at the rearward end of the curved body may be due to sting interference. It should be noted that, at angles of attack above 12°, integration of the curves of figure 9 does not give as large a value for C_{N_F} as those plotted in figure 5. The data presented for the cylindrical body in figure 9 have been faired consistently with the data of reference 1, whereas the data of figure 5 agree with the strain-gage data of reference 2.

CONCLUSIONS

Analysis of the results obtained from a transonic wind-tunnel investigation of two bodies of revolution, one incorporating a cylindrical afterbody, the other incorporating a curved afterbody, indicates:

1. The pressures over the nose of both bodies are very similar although higher induced velocities exist over the rearward portions of the curved body; however, the cross-section normal-force coefficient is greater over the rearward portions of the cylindrical body.

2. At a given Mach number and angle of attack, the normal-force coefficient for the cylindrical body is greater than that for the curved body.

3. The center-of-pressure location was more rearward for the cylindrical body than for the curved body. Consequently, the cylindrical body exhibited more desirable stability characteristics.

4. The variation of normal-force and pitching-moment coefficients with Mach number is rather small, especially at the lower angles of attack.

5. The maximum meridian load for the cylindrical body occurs at approximately the 105° meridian.

6. The theoretical normal-force and pitching-moment characteristics of both bodies are in fair agreement with the results of this investigation.

Langley Aeronautical Laboratory,
    National Advisory Committee for Aeronautics,
        Langley Field, Va., December 9, 1953.

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TABLE I

PRESSURE DATA, CYLINDRICAL BODY

(a) M = 0.60

x, in.	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
			α = 20°						α = 16°						α = 12°			
0.50	-0.053	——	——	——	——	——	-0.002	——	——	——	——	——	0.027	——	——	——	——	——
1.50	-.062	——	——	——	——	——	-.035	——	——	——	——	——	-.025	——	——	——	——	——
2.50	-.057	-0.265	-0.304	-0.221	0.078	0.126	-.045	-0.158	-0.187	-0.100	0.109	0.300	-.031	-.085	-0.094	-0.025	0.113	0.235
3.50	-.067	——	——	——	——	——	-.051	——	——	——	——	——	-.056	——	——	——	——	——
4.50	-.070	-.161	-.342	-.268	.009	——	-.058	-.141	-.218	-.141	.041	——	-.046	-.097	-.127	-.071	.054	——
5.50	-.074	——	——	——	——	——	-.060	——	——	——	——	——	-.051	——	——	——	——	——
6.50	-.055	-.155	-.334	-.298	-.059	.155	-.065	-.141	-.228	-.179	-.007	.173	-.059	-.106	-.140	-.105	.012	.121
8.50	-.058	-.142	-.326	-.300	-.065	.156	-.049	-.126	-.230	-.190	-.052	.145	-.045	-.105	-.146	-.110	-.005	.092
10.50	-.058	-.138	-.308	-.304	-.085	.151	-.040	-.112	-.224	-.205	-.051	.121	-.042	-.093	-.147	-.121	-.022	.080
12.50	-.048	-.150	-.280	-.305	-.095	.146	-.056	-.102	-.209	-.202	-.065	.105	-.036	-.080	-.139	-.121	-.052	.065
14.50	-.046	-.124	-.292	-.308	-.106	.124	-.059	-.096	-.198	-.211	-.079	.079	-.028	-.075	-.140	-.131	-.045	.044
16.50	-.047	-.118	-.216	-.301	-.113	.125	-.056	-.084	-.176	-.211	-.086	.077	-.020	-.065	-.129	-.130	-.049	.044
17.17	-.050	——	——	——	——	——	-.057	——	——	——	——	——	-.017	——	——	——	——	——
18.17	-.058	-.105	-.191	-.294	-.115	.127	-.057	-.077	-.156	-.205	-.088	.070	-.016	-.056	-.118	-.124	-.050	.059
19.17	-.046	——	——	——	——	——	-.027	——	——	——	——	——	-.005	——	——	——	——	——
20.17	-.038	-.099	-.167	-.283	-.106	.132	-.036	-.072	-.136	-.194	-.082	.076	-.011	-.044	-.104	-.114	-.044	.048
21.17	-.056	——	-.173	-.272	-.100	——	-.032	——	-.141	-.189	-.075	——	-.006	——	-.111	-.110	-.035	——
22.17	-.030	-.094	-.164	-.266	-.097	.136	-.028	-.065	-.132	-.181	-.073	.080	-.006	-.058	-.098	-.102	-.056	.053
23.17	-.026	——	-.149	-.260	-.096	——	-.024	——	-.117	-.174	-.068	——	-.004	——	-.095	-.101	-.032	——
24.17	-.027	-.091	——	-.253	-.092	.135	-.022	-.057	——	-.168	-.065	.080	-.005	-.054	——	-.099	-.028	.054
25.17	-.029	——	——	-.256	-.095	——	-.024	——	——	-.168	-.067	——	-.008	——	-.079	-.100	-.028	——
26.17	——	-.088	——	-.248	——	.157	——	-.053	——	-.160	——	.078	——	-.051	——	-.093	-.020	.052
27.17	-.025	——	-.119	-.254	——	——	-.019	——	-.103	-.167	-.053	——	-.009	——	——	-.098	——	——
28.17	-.028	-.085	-.107	-.248	——	.158	-.018	-.051	-.078	-.167	——	.078	-.011	-.032	——	-.096	——	.054
29.17	-.054	——	——	-.251	-.084	——	-.021	——	——	-.162	——	——	-.012	——	——	-.098	——	——
30.17	-.055	-.078	——	-.244	-.081	.140	-.018	-.046	——	-.158	-.058	.082	-.010	-.028	——	-.094	-.025	.058
31.17	-.056	——	-.102	-.241	-.094	——	-.013	——	-.068	-.155	-.054	——	-.007	——	——	-.093	-.023	——
32.17	-.043	-.077	-.101	-.241	-.095	.138	-.019	-.044	-.060	-.149	-.060	.060	-.012	-.029	——	-.095	-.026	.056
33.17	-.045	——	——	——	——	——	-.019	——	——	——	——	——	-.010	——	——	——	——	——
34.17	-.047	-.075	-.096	-.239	-.092	.146	-.018	-.036	-.060	-.143	-.061	.082	-.007	-.027	-.055	-.091	-.026	.058
35.17	-.055	——	——	——	——	——	-.018	——	——	——	——	——	-.007	——	——	——	——	——
36.17	-.060	-.072	-.095	-.239	-.092	.138	-.015	-.037	-.056	-.141	-.052	.086	-.005	-.028	-.057	-.095	-.024	.061
37.17	-.067	——	——	——	——	——	-.024	——	——	——	——	——	-.007	——	——	——	——	——
38.15	-.075	-.077	-.097	-.243	-.107	.108	-.030	-.040	-.057	-.147	-.065	.058	-.010	-.034	-.063	-.104	-.037	.058
38.40	-.084	——	——	——	——	——	-.036	——	——	——	——	——	-.011	——	——	——	——	——
38.65	-.093	——	——	——	——	——	-.046	——	——	——	——	——	-.023	——	——	——	——	——
38.90	-.118	——	——	——	——	——	-.065	——	——	——	——	——	-.041	——	——	——	——	——
39.15	-.181	-.123	-.128	-.268	-.210	-.014	-.131	-.083	-.086	-.187	-.160	-.056	-.102	-.072	-.101	-.162	-.138	-.072
			α = 8°						α = 4°						α = 0°			
0.50	0.075	——	——	——	——	——	0.115	——	——	——	——	——	0.175					
1.50	.011	——	——	——	——	——	.040	——	——	——	——	——	.087					
2.50	-.004	-0.025	-0.014	0.054	0.105	0.176	.021	0.025	0.042	0.059	0.091	0.114	.049					
3.50	-.010	——	——	——	——	——	.007	——	——	——	——	——	.033					
4.50	-.023	-.041	-.049	-.012	.052	——	-.012	-.011	-.005	.014	.041	.063	.015					
5.50	-.029	——	——	——	——	——	-.022	——	——	——	——	——	-.001					
6.50	-.039	-.058	-.067	-.043	.013	.076	-.036	-.036	-.089	-.013	.004	.031	-.016					
8.50	-.054	-.057	-.073	-.052	.005	.056	-.039	-.043	-.059	-.024	-.006	.012	-.016					
10.50	-.053	-.058	-.075	-.062	-.013	.044	-.059	-.046	-.043	-.050	-.012	.005	-.027					
12.50	-.046	-.045	-.072	-.068	-.019	.054	-.058	-.042	-.041	-.052	-.003	-.029	-.029					
14.50	-.034	-.047	-.074	-.070	-.028	.020	-.039	-.045	-.047	-.040	-.028	-.017	-.034					
16.50	-.014	-.037	-.061	-.068	-.029	.022	-.051	-.059	-.041	-.058	-.026	-.007	-.028					
17.17	-.010	——	——	——	——	——	-.051	——	——	——	——	——	-.029					
18.17	-.005	-.026	-.057	-.062	-.027	.019	-.026	-.052	-.037	-.054	-.022	-.010	-.023					
19.17	.005	——	——	——	——	——	-.014	——	——	——	——	——	-.016					
20.17	.001	-.014	-.045	-.055	-.022	.027	-.015	-.020	-.026	-.027	-.016	.001	-.016					
21.17	.010	——	-.048	-.049	-.015	——	-.011	——	-.031	-.021	-.008	——	-.014					
22.17	.014	-.009	-.058	-.040	-.009	.058	-.007	-.014	-.019	-.013	-.006	.008	-.007					
23.17	.018	——	-.053	-.039	-.007	——	-.004	——	-.015	-.015	-.004	——	-.004					
24.17	.021	-.005	——	-.056	-.003	.059	-.005	-.007	-.018	-.011	-.003	.010	-.003					
25.17	.019	——	-.026	-.037	-.005	——	-.003	——	——	-.011	-.001	——	-.005					
26.17	——	-.001	——	-.050	——	.059	——	-.005	——	-.006	——	.010	-.010					
27.17	.023	——	——	-.055	.004	——	-.001	——	-.013	-.009	.001	——	-.001					
28.17	.024	.001	——	-.054	——	.045	-.001	-.004	——	-.008	——	.012	.000					
29.17	.024	——	——	-.053	——	——	-.001	——	——	-.009	——	——	-.001					
30.17	.024	.004	——	-.050	.006	.044	.000	-.002	——	-.008	.002	.014	.001					
31.17	.026	——	——	-.029	.006	——	-.001	——	——	-.006	.005	——	.001					
32.17	.023	.004	——	-.026	.004	.045	-.001	-.005	——	-.006	.004	.011	.001					
33.17	.024	——	——	——	——	——	.001	——	——	——	——	——	.000					
34.17	.027	.008	-.002	-.024	.005	.047	.001	-.001	-.005	-.005	.004	.014	.002					
35.17	.027	——	——	——	——	——	.000	——	——	——	——	——	-.001					
36.17	.030	.009	-.005	-.024	.007	.050	.002	-.005	-.007	-.008	.005	.014	-.002					
37.17	.028	——	——	——	——	——	.000	——	——	——	——	——	-.004					
38.15	.022	.003	-.009	-.052	-.001	.028	-.006	-.013	-.016	-.018	-.009	-.004	-.012					
38.40	.019	——	——	——	——	——	-.007	——	——	——	——	——	-.015					
38.65	.010	——	——	——	——	——	-.014	——	——	——	——	——	-.023					
38.90	-.005	——	——	——	——	——	-.028	——	——	——	——	——	-.036					
39.15	-.059	-.029	-.049	-.092	-.087	-.054	-.054	-.047	-.066	-.085	-.087	-.085	-.065					

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(b) M = 0.80

x, in.	α = 20° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 16° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 12° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
0.50	-0.002						0.024						0.053					
1.50	-.058						-.020						-.011					
2.50	-.053	-0.238	-0.298	-0.205	0.101	0.394	-.035	-0.127	-0.173	-0.084	0.126	0.321	-.021	-0.073	-0.085	-0.014	0.126	0.247
3.50	-.056						-.044						-.026					
4.50	-.069	-.157	-.359	-.262	.024		-.056	-.128	-.212	-.156	.054		-.042	-.087	-.116	-.063	.060	
5.50	-.071						-.057						-.048					
6.50	-.079	-.156	-.543	-.291	-.053	.252	-.066	-.132	-.251	-.181	-.005	.186	-.059	-.105	-.143	-.092	.012	.125
8.50	-.057	-.149	-.330	-.305	-.063	.212	-.049	-.120	-.230	-.198	-.033	.151	-.048	-.100	-.148	-.113	-.009	.094
10.50	-.045	-.148	-.306	-.312	-.085	.188	-.042	-.113	-.225	-.209	-.053	.127	-.042	-.093	-.150	-.122	-.025	.078
12.50	-.047	-.139	-.267	-.313	-.094	.166	-.058	-.099	-.205	-.210	-.066	.112	-.053	-.080	-.143	-.126	-.035	.064
14.50	-.060	-.133	-.238	-.317	-.109	.135	-.043	-.098	-.191	-.218	-.083	.081	-.052	-.076	-.145	-.137	-.050	.041
16.50	-.056	-.124	-.198	-.308	-.117	.134	-.056	-.089	-.163	-.213	-.088	.081	-.020	-.066	-.129	-.134	-.053	.041
17.17	-.059						-.058						-.020					
18.17	-.059	-.111	-.171	-.299	-.120	.123	-.059	-.075	-.141	-.207	-.092	.074	-.017	-.055	-.117	-.128	-.055	.055
19.17	-.046						-.026						-.004					
20.17	-.053	-.102	-.144	-.284	-.109	.132	-.035	-.065	-.113	-.190	-.080	.085	-.012	-.042	-.100	-.117	-.043	.046
21.17	-.044		-.153	-.270	-.098		-.028		-.121	-.183	-.071		-.005		-.107	-.110	-.037	
22.17	-.036	-.097	-.142	-.265	-.096	.137	-.025	-.062	-.110	-.171	-.070	.089	-.004	-.038	-.095	-.100	-.055	.053
23.17	-.031		-.129	-.257	-.094		-.022		-.095	-.167	-.067		-.004		-.087	-.099	-.032	
24.17	-.023	-.090		-.253	-.085	.158	-.020	-.055		-.161	-.059	.092	-.004	-.054		-.095	-.026	.057
25.17	-.027			-.254	-.089		-.024			-.163	-.060		-.006		-.073	-.096	-.027	
26.17		-.090		-.243		.136		-.052		-.153		.089		-.050		-.090		.055
27.17	-.022		-.110	-.249	-.076		-.016		-.082	-.157			-.006			-.092	-.019	
28.17	-.024	-.089	-.096	-.245		.137	-.020	-.047	-.064	-.157	-.051	.091	-.008	-.029		-.093		.058
29.17	-.029			-.251			-.019			-.157			-.011			-.094		
30.17	-.029	-.082		-.239	-.085	.142	-.018	-.045		-.149	-.053	.094	-.006	-.026		-.091	-.024	.060
31.17	-.028		-.094	-.236	-.079		-.014		-.054	-.145	-.049		-.006			-.088	-.021	
32.17	-.034	-.081	-.093	-.237	-.089	.138	-.018	-.041	-.049	-.145	-.054	.093	-.011	-.025		-.089	-.026	.059
33.17	-.035						-.016						-.008					
34.17	-.035	-.077	-.091	-.236	-.094	.139	-.015	-.036	-.045	-.140	-.054	.095	-.005	-.025	-.050	-.089	-.028	.059
35.17	-.041						-.016						-.003					
36.17	-.044	-.077	-.092	-.236	-.086	.145	-.016	-.037	-.045	-.141	-.047	.097	-.002	-.027	-.054	-.090	-.024	.063
37.17	-.049						-.021						-.005					
38.15	-.057	-.084	-.093	-.245	-.104	.115	-.025	-.042	-.051	-.146	-.063	.071	-.007	-.033	-.069	-.105	-.040	.036
38.40	-.063						-.029						-.012					
38.65	-.075						-.041						-.020					
38.90	-.100						-.061						-.059					
39.15	-.175	-.135	-.127	-.268	-.217	-.027	-.130	-.090	-.088	-.191	-.171	-.067	-.104	-.080	-.104	-.173	-.156	-.094

x, in.	α = 8° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 4° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 0° θ=0°
0.50	0.094						0.142						0.198
1.50	.018						.056						.104
2.50	-.003	-0.018	-0.010	0.059	0.116	0.184	.027	0.036	0.053	0.068	0.099	0.125	.062
3.50	-.010						.013						.041
4.50	-.028	-.059	-.044	-.010	.055		-.005	-.002	.005	.020	.044	.068	.021
5.50	-.036						-.019						.005
6.50	-.050	-.063	-.075	-.040	.010	.073	-.035	-.054	-.027	-.010	.009	.051	-.012
8.50	-.046	-.066	-.083	-.058	-.003	.053	-.056	-.041	-.059	-.027	-.008	.009	-.016
10.50	-.045	-.065	-.085	-.068	-.018	.058	-.040	-.046	-.045	-.035	-.018	.002	-.026
12.50	-.037	-.055	-.079	-.071	-.024	.050	-.038	-.041	-.042	-.036	-.022	-.004	-.026
14.50	-.035	-.055	-.083	-.080	-.036	.009	-.041	-.046	-.048	-.046	-.031	-.021	-.035
16.50	-.024	-.045	-.072	-.075	-.036	.012	-.030	-.059	-.042	-.042	-.029	-.015	-.030
17.17	-.022						-.050						-.028
18.17	-.016	-.035	-.065	-.071	-.054	.011	-.026	-.030	-.035	-.058	-.028	-.015	-.027
19.17	-.002						-.015						-.013
20.17	-.004	-.019	-.050	-.058	-.025	.024	-.014	-.018	-.025	-.028	-.020	-.002	-.013
21.17	.003		-.056	-.051	-.016		-.009		-.051	-.021	-.012		-.009
22.17	.008	-.013	-.061	-.044	-.014	.034	-.003	-.013	-.018	-.015	-.010	.008	-.005
23.17	.012		-.038	-.043	-.011		.000		-.015	-.011	-.005		-.001
24.17	.012	-.007		-.039	-.006	.036	.001	-.006	-.014	-.010	-.004	.010	.000
25.17	.013		-.029	-.040	-.006		.001			-.009	-.001		.001
26.17		-.005		-.053		.057		-.005		-.008		.006	
27.17	.018			-.055	.002		.001		-.014	-.012	.002		.002
28.17	.019	-.003		-.056		.040	.003	-.004		-.010		.011	.002
29.17	.016			-.055			.001			-.011			.002
30.17	.018	.000		-.053	.001	.044	.004	-.001		-.009	.001	.014	.005
31.17	.019			-.028	.003		.003			-.008	.002		.003
32.17	.015	.002		-.028	.005	.044	.001	-.001		-.007	.002	.012	.004
33.17	.017						.003						.004
34.17	.020	.004	-.007	-.026	.005	.045	.004	.000	-.005	-.006	.000	.013	.005
35.17	.022						.004						.003
36.17	.024	.005	-.009	-.025	.006	.052	.004	-.003	-.007	-.008	.000	.016	.005
37.17	.020						-.001						.000
38.15	.016	-.002	-.016	-.036	-.006	.028	-.007	-.015	-.019	-.023	-.014	-.007	-.008
38.40	.013						-.011						-.014
38.65	.006						-.020						-.024
38.90	-.009						-.028						-.040
39.15	-.067	-.059	-.060	-.108	-.108	-.086	-.058	-.051	-.074	-.099	-.105	-.105	-.068

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(c) M = 0.85

Pressure coefficients of row -

x, in.	α = 20° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 16° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 12° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
0.50	0.005	----	----	----	----	----	0.055	----	----	----	----	----	0.062	----	----	----	----	----
1.50	-.041						-.014						-.006					
2.50	-.054	-0.229	-0.295	-0.199	0.109	0.402	-.052	-0.125	-0.171	-0.079	0.153	0.328	-.017	-0.071	-0.034	-0.010	0.128	0.252
3.50	-.060						-.041						-.023					
4.50	-.074	-.158	-.341	-.260	..027	----	-.054	-.128	-.212	-.132	.057	----	-.042	-.088	-.116	-.062	.063	----
5.50	-.078						-.058						-.050					
6.50	-.089	-.160	-.349	-.292	-.051	.252	-.067	-.133	-.254	-.180	.000	.188	-.061	-.108	-.147	-.097	.016	.124
8.50	-.066	-.156	-.337	-.311	-.062	.213	-.050	-.123	-.233	-.199	-.035	.150	-.049	-.105	-.155	-.117	-.013	.096
10.50	-.054	-.155	-.309	-.317	-.084	.188	-.045	-.115	-.226	-.209	-.053	.125	-.045	-.096	-.157	-.129	-.029	.075
12.50	-.054	-.145	-.268	-.318	-.098	.166	-.059	-.105	-.208	-.212	-.068	.110	-.054	-.082	-.147	-.132	-.040	.061
14.50	-.069	-.141	-.255	-.324	-.113	.152	-.044	-.102	-.195	-.222	-.086	.078	-.052	-.080	-.148	-.142	-.055	.056
16.50	-.067	-.129	-.196	-.312	-.119	.129	-.059	-.091	-.165	-.217	-.090	.079	-.022	-.069	-.132	-.138	-.053	.057
17.17	-.070						-.041						-.023					
18.17	-.070	-.116	-.169	-.305	-.124	.121	-.042	-.079	-.144	-.209	-.094	.072	-.021	-.058	-.120	-.135	-.061	.052
19.17	-.055						-.026						-.006					
20.17	-.065	-.107	-.141	-.286	-.110	.130	-.058	-.066	-.113	-.191	-.085	.085	-.014	-.043	-.099	-.122	-.048	.044
21.17	-.051	----	-.151	-.271	-.101	----	-.050	----	-.122	-.179	-.072	----	-.006	----	-.108	-.113	-.040	----
22.17	-.044	-.101	-.139	-.266	-.100	.136	-.026	-.060	-.110	-.170	-.069	.091	-.005	-.040	-.094	-.104	-.037	.052
23.17	-.059	----	-.128	-.259	-.097	----	-.024	----	-.094	-.168	-.066	----	-.004	----	-.087	-.100	-.055	----
24.17	-.052	-.095	----	-.254	-.087	.137	-.019	-.054	----	-.164	-.059	.091	-.004	-.055	----	-.098	-.028	.052
25.17	-.053	----	----	-.254	-.090	----	-.022	----	----	-.163	-.060	----	-.007	----	-.073	-.099	-.050	----
26.17	----	-.091	----	-.245	----	.137	----	-.052	----	-.154	----	.090	----	-.053	----	-.092	----	.053
27.17	-.028	----	-.111	-.250	-.082	----	-.017	----	-.085	-.155	-.051	----	-.007	----	----	-.095	-.023	----
28.17	-.029	-.091	-.099	-.249	----	.138	-.020	-.048	-.063	-.155	----	.091	-.009	-.052	----	-.097	----	.052
29.17	-.035	----	----	-.251	----	----	-.019	----	----	-.157	----	----	-.012	----	----	-.096	----	----
30.17	-.033	-.086	----	-.243	-.085	.142	-.017	-.044	----	-.152	-.054	.095	-.008	-.029	----	-.094	-.028	.057
31.17	-.031	----	-.095	-.259	-.082	----	-.013	----	-.056	-.147	-.048	----	-.006	----	----	-.092	-.024	----
32.17	-.039	-.086	-.095	-.241	-.092	.140	-.018	-.042	-.050	-.146	-.055	.093	-.011	-.028	----	-.092	-.027	.057
33.17	-.039						-.017						-.009					
34.17	-.040	-.082	-.095	-.238	-.095	.140	-.013	-.038	-.047	-.142	-.056	.092	-.006	-.027	-.051	-.092	-.052	.056
35.17	-.042						-.015						-.007					
36.17	-.043	-.085	-.092	-.240	-.087	.148	-.015	-.039	-.048	-.141	-.048	.098	-.005	-.031	-.054	-.092	-.027	.061
37.17	-.051						-.020						-.007					
38.15	-.057	-.090	-.098	-.252	-.107	.116	-.024	-.047	-.057	-.150	-.064	.068	-.011	-.041	-.065	-.109	-.045	.054
38.40	-.063						-.027						-.013					
38.65	-.073						-.059						-.022					
38.90	-.096						-.059						-.041					
39.15	-.173	-.139	-.131	-.275	-.231	-.055	-.130	-.095	-.092	-.200	-.182	-.077	-.109	-.085	-.108	-.180	-.167	-.106

x, in.	α = 8° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 4° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 0° θ=0°
0.50	0.105	----	----	----	----	----	0.153	----	----	----	----	----	0.209
1.50	.024						.066						.112
2.50	.000	-0.014	-0.006	0.044	0.120	0.187	.054	0.041	0.056	0.073	0.105	0.130	.069
3.50	-.007						.021						.047
4.50	-.025	-.058	-.042	-.009	----	----	.000	.000	.005	.028	.049	.073	.025
5.50	-.057						-.015						.006
6.50	-.049	-.066	-.075	-.042	.010	.072	-.033	-.053	-.027	-.007	.013	.051	-.010
8.50	-.047	-.069	-.084	-.061	-.005	.053	-.056	-.042	-.059	-.025	-.009	.010	-.015
10.50	-.046	-.068	-.088	-.070	-.020	.055	-.041	-.046	-.045	-.033	-.017	.001	-.025
12.50	-.058	-.060	-.082	-.073	-.027	.028	-.056	-.042	-.043	-.033	-.021	-.005	-.026
14.50	-.058	-.059	-.086	-.065	-.041	.006	-.041	-.047	-.050	-.045	-.031	-.022	-.055
16.50	-.024	-.048	-.075	-.079	-.041	.009	-.052	-.040	-.043	-.042	-.029	-.015	-.050
17.17	-.022						-.050						-.028
18.17	-.018	-.037	-.066	-.076	-.059	.009	-.025	-.051	-.056	-.057	-.028	-.015	-.025
19.17	-.002						-.013						-.014
20.17	-.006	-.022	-.049	-.060	-.028	.025	-.011	-.015	-.025	-.026	-.018	-.001	-.013
21.17	.005	----	-.056	-.051	-.016	----	-.008	----	-.032	-.017	-.009	----	-.008
22.17	.008	-.015	-.041	-.045	-.013	.053	.000	-.011	-.016	-.012	-.006	.010	-.002
23.17	.013	----	-.059	-.043	-.011	----	.002	----	-.013	-.010	-.002	1	-.002
24.17	.015	-.009	----	-.041	-.007	.034	.003	-.006	-.013	-.008	-.002	.012	.004
25.17	.013	----	-.050	-.040	-.006	----	.005	----	----	-.006	.001	----	.002
26.17	----	-.006	----	-.055	----	.056	----	-.005	----	-.007	----	.011	----
27.17	.017	----	----	-.054	.000	----	.004	----	-.012	-.009	.004	----	.005
28.17	.016	-.005	----	-.053	----	.040	.005	-.002	----	-.006	----	.014	.004
29.17	.015	----	----	-.056	----	----	.004	----	----	-.007	----	----	.005
30.17	.018	-.001	----	-.054	.000	.044	.006	.001	----	-.006	.005	.018	.006
31.17	.018	----	----	-.051	.003	----	.006	----	----	-.004	.005	----	.005
32.17	.016	.000	----	-.089	.002	.046	.005	-.001	----	-.005	.005	.016	.004
33.17	.017						.006						.004
34.17	.020	.005	-.006	-.029	.002	.046	.006	.000	-.005	-.004	.005	.016	.007
35.17	.017						.004						.004
36.17	.019	.008	-.010	-.029	.005	.051	.004	-.005	-.006	-.006	.004	.018	.005
37.17	.013						.000						.000
38.15	.012	-.006	-.019	-.041	-.007	.029	-.007	-.015	-.019	-.022	-.012	-.004	-.011
38.40	.010						-.011						-.015
38.65	.001						-.018						-.027
38.90	-.016						-.050						-.044
39.15	-.071	-.043	-.067	-.114	-.116	-.095	-.058	-.053	-.077	-.105	-.110	-.110	-.072

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(d) M = 0.90

x, in.	Pressure coefficients of row —																	
	$\theta=0°$	$\theta=45°$	$\theta=75°$	$\theta=105°$	$\theta=135°$	$\theta=180°$	$\theta=0°$	$\theta=45°$	$\theta=75°$	$\theta=105°$	$\theta=135°$	$\theta=180°$	$\theta=0°$	$\theta=45°$	$\theta=75°$	$\theta=105°$	$\theta=135°$	$\theta=180°$
	$\alpha=20°$						$\alpha=16°$						$\alpha=12°$					
0.50	0.019	-----	-----	-----	-----	-----	0.047	-----	-----	-----	-----	-----	0.076	-----	-----	-----	-----	-----
1.50	-.034	-----	-----	-----	-----	-----	-.007	-----	-----	-----	-----	-----	.002	-----	-----	-----	-----	-----
2.50	-.051	-0.218	-0.288	-0.186	0.120	0.407	-.028	-0.115	-0.165	-0.068	0.141	0.334	-.013	-0.065	-0.076	-0.002	0.136	0.259
3.50	-.058	-----	-----	-----	-----	-----	-.039	-----	-----	-----	-----	-----	-.018	-----	-----	-----	-----	-----
4.50	-.074	-.158	-.340	-.253	.036	-----	-.055	-.126	-.210	-.189	.061	-----	-.041	-.085	-.113	-.056	.067	-----
5.50	-.081	-----	-----	-----	-----	-----	-.060	-----	-----	-----	-----	-----	-.050	-----	-----	-----	-----	-----
6.50	-.091	-.164	-.355	-.294	-.030	.255	-.070	-.136	-.256	-.182	-.002	.187	-.063	-.108	-.147	-.097	.016	.128
8.50	-.069	-.162	-.342	-.316	-.064	.214	-.055	-.126	-.239	-.204	-.054	.150	-.052	-.106	-.137	-.120	-.013	.095
10.50	-.059	-.162	-.314	-.325	-.086	.185	-.049	-.120	-.230	-.215	-.059	.122	-.048	-.100	-.138	-.130	-.052	.073
12.50	-.060	-.153	-.268	-.327	-.105	.164	-.042	-.108	-.211	-.219	-.073	.106	-.058	-.085	-.149	-.133	-.042	.058
14.50	-.074	-.149	-.236	-.389	-.121	.127	-.049	-.107	-.198	-.230	-.091	.072	-.058	-.085	-.151	-.147	-.058	.053
16.50	-.071	-.136	-.195	-.318	-.129	.125	-.043	-.096	-.169	-.223	-.097	.073	-.027	-.073	-.136	-.142	-.062	.053
17.17	-.073	-----	-----	-----	-----	-----	-.045	-----	-----	-----	-----	-----	-.025	-----	-----	-----	-----	-----
18.17	-.073	-.123	-.169	-.310	-.134	.116	-.044	-.085	-.144	-.214	-.100	.066	-.022	-.061	-.121	-.135	-.062	.028
19.17	-.059	-----	-----	-----	-----	-----	-.028	-----	-----	-----	-----	-----	-.007	-----	-----	-----	-----	-----
20.17	-.067	-.110	-.136	-.286	-.116	.129	-.042	-.058	-.111	-.196	-.085	.080	-.016	-.045	-.100	-.121	-.050	.044
21.17	-.055	-----	-.145	-.264	-.099	-----	-.054	-----	-.120	-.185	-.076	-----	-.008	-----	-.109	-.111	-.040	-----
22.17	-.047	-.103	-.134	-.262	-.099	.153	-.027	-.062	-.107	-.172	-.073	.087	-.005	-.038	-.092	-.101	-.037	.055
23.17	-.040	-----	-.125	-.260	-.097	-----	-.026	-----	-.094	-.168	-.070	-----	-.004	-----	-.085	-.101	-.033	-----
24.17	-.053	-.095	-----	-.255	-.086	.138	-.022	-.056	-----	-.165	-.061	.089	-.004	-.035	-----	-.097	-.028	.053
25.17	-.035	-----	-----	-.253	-.088	-----	-.024	-----	-----	-.164	-.063	-----	-.007	-----	-.070	-.097	-.029	-----
26.17	-----	-.095	-----	-.247	-----	.136	-----	-.053	-----	-.159	-----	.088	-----	-.053	-----	-.090	-----	.052
27.17	-.028	-----	-.110	-.247	-.082	-----	-.019	-----	-.082	-.158	-.054	-----	-.007	-----	-----	-.090	-.022	-----
28.17	-.050	-.093	-.099	-.242	-----	.138	-.021	-.050	-.065	-.159	-----	.090	-.009	-.032	-----	-.093	-----	.055
29.17	-.033	-----	-----	-.249	-----	-----	-.021	-----	-----	-.161	-----	-----	-.012	-----	-----	-.098	-----	-----
30.17	-.050	-.088	-----	-.242	-.084	.142	-.019	-.047	-----	-.153	-.058	.095	-.007	-.028	-----	-.095	-.028	.058
31.17	-.052	-----	-.097	-.254	-.079	-----	-.015	-----	-.056	-.147	-.051	-----	-.008	-----	-----	-.089	-.024	-----
32.17	-.038	-.088	-.095	-.258	-.088	.140	-.019	-.046	-.053	-.148	-.056	.092	-.011	-.029	-----	-.089	-.028	.057
33.17	-.039	-----	-----	-----	-----	-----	-.019	-----	-----	-----	-----	-----	-.009	-----	-----	-----	-----	-----
34.17	-.054	-.084	-.095	-.240	-.095	.138	-.016	-.040	-.049	-.145	-.058	.092	-.006	-.028	-.050	-.090	-.029	.057
35.17	-.043	-----	-----	-----	-----	-----	-.015	-----	-----	-----	-----	-----	-.007	-----	-----	-----	-----	-----
36.17	-.045	-.086	-.095	-.242	-.088	.146	-.014	-.042	-.050	-.145	-.052	.097	-.006	-.031	-.054	-.090	-.026	.063
37.17	-.049	-----	-----	-----	-----	-----	-.022	-----	-----	-----	-----	-----	-.010	-----	-----	-----	-----	-----
38.15	-.053	-.097	-.106	-.255	-.189	.116	-.024	-.050	-.060	-.157	-.067	.068	-.013	-.043	-.068	-.110	-.043	.035
38.40	-.058	-----	-----	-----	-----	-----	-.029	-----	-----	-----	-----	-----	-.017	-----	-----	-----	-----	-----
38.65	-.069	-----	-----	-----	-----	-----	-.038	-----	-----	-----	-----	-----	-.023	-----	-----	-----	-----	-----
38.90	-.090	-----	-----	-----	-----	-----	-.055	-----	-----	-----	-----	-----	-.040	-----	-----	-----	-----	-----
39.15	-.162	-.145	-.136	-.286	-.266	-.040	-.126	-.102	-.097	-.213	-.200	-.083	-.111	-.091	-.111	-.195	-.180	-.111

x, in.	Pressure coefficients of row —													
	$\theta=0°$	$\theta=45°$	$\theta=75°$	$\theta=105°$	$\theta=135°$	$\theta=180°$	$\theta=0°$	$\theta=45°$	$\theta=75°$	$\theta=105°$	$\theta=135°$	$\theta=180°$	$\theta=0°$
	$\alpha=8°$						$\alpha=4°$						$\alpha=0°$
0.50	0.115	-----	-----	-----	-----	-----	0.166	-----	-----	-----	-----	-----	0.221
1.50	.032	-----	-----	-----	-----	-----	.073	-----	-----	-----	-----	-----	.120
2.50	.004	-0.006	0.001	0.050	0.126	0.194	.040	0.048	0.064	0.079	0.109	0.136	.073
3.50	-.004	-----	-----	-----	-----	-----	.024	-----	-----	-----	-----	-----	.051
4.50	-.023	-.035	-.059	-.005	.062	-----	.000	.004	.010	.027	.051	.076	.028
5.50	-.056	-----	-----	-----	-----	-----	-.016	-----	-----	-----	-----	-----	.007
6.50	-.052	-.068	-.076	-.040	.011	.072	-.056	-.035	-.028	-.012	.012	.031	-.012
8.50	-.050	-.069	-.087	-.059	-.005	.052	-.059	-.043	-.040	-.030	-.010	.007	-.015
10.50	-.049	-.071	-.090	-.070	-.024	.053	-.044	-.048	-.047	-.038	-.021	-.002	-.028
12.50	-.041	-.060	-.084	-.074	-.029	.025	-.040	-.043	-.044	-.038	-.024	-.006	-.028
14.50	-.043	-.061	-.091	-.087	-.043	.005	-.046	-.049	-.054	-.051	-.026	-.026	-.040
16.50	-.031	-.051	-.079	-.081	-.042	.007	-.055	-.041	-.045	-.045	-.033	-.018	-.033
17.17	-.026	-----	-----	-----	-----	-----	-.053	-----	-----	-----	-----	-----	-.031
18.17	-.021	-.038	-.069	-.077	-.041	.005	-.028	-.032	-.037	-.040	-.030	-.018	-.029
19.17	-.006	-----	-----	-----	-----	-----	-.016	-----	-----	-----	-----	-----	-.015
20.17	-.009	-.021	-.051	-.062	-.029	.020	-.013	-.015	-.024	-.027	-.019	-.002	-.014
21.17	.000	-----	-.060	-.053	-.019	-----	-.009	-----	-.033	-.019	-.010	-----	-.010
22.17	.006	-.017	-.043	-.046	-.017	-.050	-.005	-.011	-.014	-.013	-.007	.011	-.002
23.17	.010	-----	-.040	-.043	-.015	-----	.001	-----	-.013	-.010	-.004	-----	.002
24.17	.012	-.012	-----	-.040	-.010	.035	.002	-.004	-.013	-.009	-.002	.013	.003
25.17	.011	-----	-.051	-.040	-.008	-----	.002	-----	-----	-.008	.000	-----	.002
26.17	-----	-.008	-----	-.035	-----	.052	-----	-.002	-----	-.006	-----	.010	-----
27.17	.013	-----	-----	-.056	-.002	-----	.005	-----	-.014	-.008	.003	-----	.003
28.17	.013	-.007	-----	-.057	-----	.056	.005	-.001	-----	-.007	-----	.013	.004
29.17	.012	-----	-----	-.058	-----	-----	.002	-----	-----	-.008	-----	-----	.003
30.17	.015	-.004	-----	-.054	-.003	.040	.005	.002	-----	-.007	.001	.016	.007
31.17	.015	-----	-----	.032	.000	-----	.005	-----	-----	-.005	.004	-----	.004
32.17	.011	-.002	-----	-.051	-.003	.041	.002	.001	-----	-.004	.003	.024	.005
33.17	.013	-----	-----	-----	-----	-----	.003	-----	-----	-----	-----	-----	.005
34.17	.015	.002	-.013	-.029	-.003	.041	.005	.001	-.005	-.006	.005	.015	.006
35.17	.015	-----	-----	-----	-----	-----	.005	-----	-----	-----	-----	-----	.002
36.17	.017	.000	-.014	-.029	.002	.047	.005	-.003	-.007	-.009	.005	.017	.005
37.17	.012	-----	-----	-----	-----	-----	-.001	-----	-----	-----	-----	-----	.002
38.15	.007	-.010	-.025	-.043	-.012	.023	-.010	-.018	-.021	-.026	-.014	-.006	-.015
38.40	.005	-----	-----	-----	-----	-----	-.015	-----	-----	-----	-----	-----	-.021
38.65	-.002	-----	-----	-----	-----	-----	-.021	-----	-----	-----	-----	-----	-.053
38.90	-.019	-----	-----	-----	-----	-----	-.035	-----	-----	-----	-----	-----	-.049
39.15	-.078	-.050	-.076	-.127	-.152	-.109	-.062	-.057	-.082	-.112	-.122	-.119	-.079

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(a) M = 0.95

x, in.	Pressure coefficients of row -
	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
	\multicolumn{6}{c}{α = 20°}	\multicolumn{6}{c}{α = 16°}	\multicolumn{6}{c}{α = 12°}
0.50	0.041	-----	-----	-----	-----	-----	0.062	-----	-----	-----	-----	-----	0.094	-----	-----	-----	-----	-----
1.50	-.021	-----	-----	-----	-----	-----	.000	-----	-----	-----	-----	-----	-.013	-----	-----	-----	-----	-----
2.50	-.040	-0.200	-0.278	-0.170	0.134	0.421	-.022	-0.107	-0.153	-0.057	0.151	0.342	-.006	-0.056	-0.066	0.007	0.146	0.266
3.50	-.052	-----	-----	-----	-----	-----	-.038	-----	-----	-----	-----	-----	-.012	-----	-----	-----	-----	-----
4.50	-.069	-.155	-.331	-.244	.046	-----	-.056	-.123	-.207	-.119	.067	-----	-.058	-.081	-.108	-.050	.073	-----
5.50	-.080	-----	-----	-----	-----	-----	-.065	-----	-----	-----	-----	-----	-.052	-----	-----	-----	-----	-----
6.50	-.097	-.170	-.359	-.294	-.024	.257	-.079	-.140	-.240	-.184	.000	.187	-.063	-.115	-.152	-.096	.018	.128
8.50	-.079	-.169	-.350	-.316	-.065	.215	-.065	-.134	-.245	-.208	-.057	.148	-.059	-.112	-.163	-.121	-.016	.093
10.50	-.066	-.168	-.317	-.341	-.096	.180	-.061	-.127	-.238	-.226	-.065	.117	-.056	-.106	-.165	-.137	-.057	.069
12.50	-.062	-.160	-.266	-.345	-.108	.157	-.055	-.116	-.215	-.226	-.080	.098	-.055	-.092	-.154	-.139	-.048	.054
14.50	-.082	-.156	-.238	-.357	-.126	.122	-.062	-.117	-.206	-.242	-.102	.066	-.046	-.093	-.160	-.157	-.069	.025
16.50	-.072	-.142	-.194	-.342	-.134	.119	-.053	-.102	-.173	-.233	-.106	.066	-.052	-.080	-.143	-.149	-.069	.026
17.17	-.078	-----	-----	-----	-----	-----	-.055	-----	-----	-----	-----	-----	-.050	-----	-----	-----	-----	-----
18.17	-.076	-.127	-.166	-.326	-.139	.108	-.052	-.088	-.147	-.223	-.108	.058	-.027	-.068	-.127	-.143	-.070	.025
19.17	-.061	-----	-----	-----	-----	-----	-.055	-----	-----	-----	-----	-----	-.010	-----	-----	-----	-----	-----
20.17	-.068	-.113	-.134	-.299	-.119	.123	-.053	-.071	-.111	-.201	-.090	.075	-.020	-.047	-.101	-.124	-.053	.040
21.17	-.064	-----	-.150	-.269	-.108	-----	-.041	-----	-.122	-.179	-.078	-----	-.010	-----	-.112	-.112	-.042	-----
22.17	-.046	-.107	-.136	-.263	-.104	.130	-.053	-.064	-.104	-.169	-.078	.085	-.006	-.042	-.092	-.101	-.058	.049
23.17	-.042	-----	-.123	-.263	-.099	-----	-.032	-----	-.091	-.169	-.072	-----	-.006	-----	-.085	-.101	-.035	-----
24.17	-.058	-.098	-----	-.258	-.092	.134	-.028	-.057	-----	-.156	-.063	.088	-.004	-.056	-----	-.097	-.030	.053
25.17	-.037	-----	-----	-.259	-.096	-----	-.031	-----	-----	-.154	-.066	-----	-.009	-----	-.070	-.098	-.050	-----
26.17	-----	-.096	-----	-.248	-----	.131	-----	-.055	-----	-.158	-----	.086	-----	-.054	-----	-.092	-----	.051
27.17	-.029	-----	-.117	-.258	-.084	-----	-.025	-----	-.085	-.153	-.054	-----	-.010	-----	-.089	-.089	-.022	-----
28.17	-.051	-.096	-.105	-.259	-----	.133	-.026	-.053	-.067	-.161	-----	.069	-.012	-.054	-----	-.095	-----	.055
29.17	-.055	-----	-----	-.256	-----	-----	-.029	-----	-----	-.161	-----	-----	-.004	-----	-----	-.097	-----	-----
30.17	-.053	-.091	-----	-.246	-.091	.136	-.024	-.050	-----	-.157	-.057	.090	-.010	-.050	-----	-.093	-.028	.056
31.17	-.051	-----	-.100	-.246	-.084	-----	-.021	-----	-.059	-.151	-.054	-----	-.010	-----	-----	-.091	-.026	-----
32.17	-.058	-.092	-.101	-.246	-.097	.134	-.025	-.050	-.057	-.151	-.060	.088	-.013	-.052	-----	-.092	-.050	.056
33.17	-.040	-----	-----	-----	-----	-----	-.025	-----	-----	-----	-----	-----	-.013	-----	-----	-----	-----	-----
34.17	-.058	-.090	-.099	-.246	-.100	.137	-.023	-.043	-.055	-.147	-.061	.089	-.010	-.051	-.052	-.092	-.051	.055
35.17	-.044	-----	-----	-----	-----	-----	-.017	-----	-----	-----	-----	-----	-.014	-----	-----	-----	-----	-----
36.17	-.045	-.092	-.102	-.252	-.095	.142	-.015	-.047	-.058	-.148	-.053	.095	-.011	-.054	-.056	-.094	-.029	.063
37.17	-.051	-----	-----	-----	-----	-----	-.023	-----	-----	-----	-----	-----	-.016	-----	-----	-----	-----	-----
38.15	-.057	-.104	-.118	-.267	-.112	.112	-.027	-.058	-.072	-.163	-.069	.069	-.020	-.052	-.073	-.112	-.043	.059
38.40	-.059	-----	-----	-----	-----	-----	-.028	-----	-----	-----	-----	-----	-.022	-----	-----	-----	-----	-----
38.65	-.064	-----	-----	-----	-----	-----	-.033	-----	-----	-----	-----	-----	-.030	-----	-----	-----	-----	-----
38.90	-.080	-----	-----	-----	-----	-----	-.048	-----	-----	-----	-----	-----	-.043	-----	-----	-----	-----	-----
39.15	-.159	-.159	-.146	-.362	-.251	-.089	-.102	-.115	-.114	-.267	-.202	-.065	-.101	-.102	-.130	-.227	-.178	-.092

x, in.	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
	\multicolumn{6}{c}{α = 8°}	\multicolumn{6}{c}{α = 4°}	\multicolumn{6}{c}{α = 0°}
0.50	0.131	-----	-----	-----	-----	-----	0.180	-----	-----	-----	-----	-----	0.235					
1.50	.042	-----	-----	-----	-----	-----	.061	-----	-----	-----	-----	-----	.151					
2.50	.011	0.000	0.008	0.056	0.135	0.201	.048	0.055	0.071	0.086	0.117	0.142	.062					
3.50	.002	-----	-----	-----	-----	-----	-.025	-----	-----	-----	-----	-----	.057					
4.50	-.021	-.032	-.056	-.001	.067	-----	.001	.006	.011	.050	.055	.078	.034					
5.50	-.058	-----	-----	-----	-----	-----	-.018	-----	-----	-----	-----	-----	.009					
6.50	-.058	-.072	-.079	-.044	.010	.071	-.041	-.037	-.052	-.014	.011	.029	-.013					
8.50	-.056	-.077	-.092	-.065	-.010	.048	-.045	-.048	-.047	-.035	-.014	.006	-.019					
10.50	-.059	-.080	-.098	-.079	-.029	.027	-.054	-.057	-.055	-.059	-.026	-.007	-.035					
12.50	-.050	-.069	-.092	-.080	-.034	.019	-.047	-.050	-.050	-.051	-.028	-.011	-.034					
14.50	-.053	-.074	-.101	-.096	-.056	-.009	-.056	-.061	-.064	-.059	-.049	-.056	-.047					
16.50	-.059	-.061	-.090	-.090	-.052	-.002	-.046	-.050	-.055	-.052	-.042	-.026	-.059					
17.17	-.055	-----	-----	-----	-----	-----	-.044	-----	-----	-----	-----	-----	-.058					
18.17	-.089	-.047	-.079	-.085	-.051	-.004	-.058	-.058	-.046	-.047	-.038	-.025	-.054					
19.17	-.011	-----	-----	-----	-----	-----	-.022	-----	-----	-----	-----	-----	-.020					
20.17	-.013	-.028	-.057	-.066	-.054	.015	-.018	-.017	-.026	-.029	-.023	-.005	-.018					
21.17	-.005	-----	-.065	-.055	-.025	-----	-.014	-----	-.056	-.021	-.011	-----	-.013					
22.17	.005	-.020	-.048	-.048	-.018	.027	-.006	-.012	-.016	-.012	-.006	.007	-.005					
23.17	.007	-----	-.044	-.045	-.016	-----	-.001	-----	-.014	-.012	-.004	-----	.000					
24.17	.009	-.016	-----	-.044	-.012	.030	-.001	-.004	-.013	-.011	-.002	.011	.002					
25.17	.007	-----	-.056	-.044	-.011	-----	-.001	-----	-----	-.008	.000	-----	.002					
26.17	-----	-.015	-----	-.058	-----	.050	-----	-.004	-----	-.006	-----	.010	-----					
27.17	.008	-----	-----	-.057	-.006	-----	-.001	-----	-.017	-.007	-.001	-----	.001					
28.17	.008	-.014	-----	-.040	-----	.053	-.001	-.004	-----	-.007	-----	.013	.002					
29.17	.006	-----	-----	-.042	-----	-----	-.001	-----	-----	-.008	-----	-----	.002					
30.17	.011	-.010	-----	-.058	-.008	.056	.002	-.001	-----	-.008	-.001	.014	.006					
31.17	.009	-----	-----	-.055	-.005	-----	-.001	-----	-----	-.005	.003	-----	.002					
32.17	.005	-.010	-----	-.054	-.006	.056	-.001	-.004	-----	-.006	.002	.015	.001					
33.17	.005	-----	-----	-----	-----	-----	.000	-----	-----	-----	-----	-----	.002					
34.17	.010	-.008	-.019	-.055	-.007	.058	.002	-.003	-.007	-.008	.001	.015	.004					
35.17	.005	-----	-----	-----	-----	-----	.002	-----	-----	-----	-----	-----	.001					
36.17	.006	-.010	-.022	-.056	-.004	.043	-.001	-.006	-.010	-.012	.001	.015	.001					
37.17	.001	-----	-----	-----	-----	-----	-.006	-----	-----	-----	-----	-----	-.006					
38.15	-.005	-.024	-.037	-.052	-.017	.022	-.017	-.026	-.031	-.050	-.016	-.006	-.020					
38.40	-.007	-----	-----	-----	-----	-----	-.020	-----	-----	-----	-----	-----	-.027					
38.65	-.016	-----	-----	-----	-----	-----	-.030	-----	-----	-----	-----	-----	-.040					
38.90	-.050	-----	-----	-----	-----	-----	-.044	-----	-----	-----	-----	-----	-.061					
39.15	-.090	-.066	-.099	-.161	-.150	-.105	-.071	-.098	-.102	-.134	-.141	-.136	-.095					

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(f) M = 0.98

Pressure coefficients of row —

x, in.	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°
	α = 20°						α = 16°						α = 12°					
0.50	0.060	-----	-----	-----	-----	-----	0.088	-----	-----	-----	-----	-----	0.111	-----	-----	-----	-----	-----
1.50	-.009						.020						.025					
2.50	-.030	-0.185	-0.265	-0.154	0.150	0.433	-.003	-0.095	-0.140	-0.059	0.167	0.356	.005	-0.042	-0.053	0.022	0.155	0.276
3.50	-.044						-.023						-.005					
4.50	-.062	-.141	-.319	-.256	.058	-----	-.043	-.117	-.197	-.111	.079	-----	-.032	-.072	-.098	-.044	.080	-----
5.50	-.078						-.053						-.046					
6.50	-.099	-.169	-.348	-.296	-.017	.261	-.079	-.147	-.238	-.177	.006	.194	-.070	-.115	-.151	-.094	.018	.130
8.50	-.080	-.168	-.355	-.329	-.062	.214	-.060	-.133	-.241	-.209	-.057	.149	-.065	-.116	-.167	-.125	-.016	.092
10.50	-.082	-.184	-.359	-.342	-.095	.180	-.074	-.146	-.259	-.244	-.071	.112	-.065	-.116	-.178	-.149	-.047	.061
12.50	-.060	-.168	-.285	-.364	-.123	.149	-.042	-.120	-.226	-.247	-.093	.091	-.047	-.095	-.161	-.144	-.054	.049
14.50	-.103	-.172	-.240	-.356	-.137	.113	-.080	-.158	-.221	-.242	-.106	.061	-.063	-.108	-.179	-.174	-.080	.013
16.50	-.092	-.162	-.217	-.359	-.139	.112	-.057	-.120	-.195	-.262	-.130	.049	-.043	-.089	-.152	-.162	-.080	.024
17.17	-.092						-.047						-.039					
18.17	-.079	-.125	-.165	-.348	-.163	.091	-.048	-.090	-.130	-.226	-.127	.046	-.051	-.071	-.132	-.156	-.063	.011
19.17	-.060						-.026						-.008					
20.17	-.064	-.121	-.142	-.288	-.112	.184	-.061	-.072	-.098	-.200	-.105	.072	-.021	-.047	-.100	-.127	-.056	.038
21.17	-.056		-.136	-.303	-.111		-.040		-.119	-.186	-.071		-.009		-.117	-.106	-.043	
22.17	-.035	-.107	-.132	-.246	-.108	.129	-.026	-.063	-.094	-.166	-.075	.084	-.004	-.040	-.087	-.099	-.043	.050
23.17	-.041		-.121	-.283	-.091		-.027		-.084	-.179	-.067		-.005		-.081	-.098	-.056	
24.17	-.046	-.098		-.250	-.093	.136	-.022	-.056		-.172	-.060	.090	-.004	-.033		-.097	-.050	.054
25.17	-.048			-.266	-.090		-.024			-.167	-.062		-.007		-.067	-.097	-.051	
26.17		-.097		-.250		.152		-.054		-.161		.087		-.033		-.095		.051
27.17	-.059		-.117	-.265	-.083		-.018		-.08	-.152	-.055		-.011			-.085	-.025	
28.17	-.054	-.097	-.106	-.262		.134	-.022	-.054	-.064	-.170		.088	-.012	-.034		-.097		.053
29.17	-.040			-.261			-.024			-.169			-.015					
30.17	-.059	-.094		-.252	-.091	.137	-.019	-.049		-.159	-.057	.090	-.010	-.031		-.095	-.050	.056
31.17	-.052		-.105	-.248	-.086		-.011		-.058	-.155	-.055		-.011			-.095	-.028	
32.17	-.056	-.095	-.104	-.251	-.094	.135	-.018	-.051	-.057	-.151	-.060	.089	-.017	-.032		-.094	-.031	.054
33.17	-.057						-.022						-.015					
34.17	-.059	-.093	-.102	-.246	-.100	.135	-.017	-.045	-.054	-.148	-.059	.089	-.013	-.032	-.050	-.094	-.052	.055
35.17	-.051						-.023						-.016					
36.17	-.052	-.096	-.106	-.253	-.092	.142	-.020	-.050	-.057	-.150	-.053	.097	-.013	-.036	-.057	-.096	-.029	.061
37.17	-.059						-.033						-.020					
38.15	-.066	-.114	-.125	-.267	-.111	.117	-.041	-.067	-.075	-.161	-.064	.074	-.031	-.057	-.075	-.111	-.040	.040
38.40	-.067						-.041						-.054					
38.65	-.074						-.052						-.042					
38.90	-.085						-.057						-.052					
39.15	-.126	-.181	-.190	-.372	-.232	-.005	-.095	-.140	-.155	-.274	-.177	-.053	-.097	-.126	-.169	-.229	-.157	-.066

x, in.	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°	θ = 0°
	α = 8°						α = 4°						α = 0°
0.50	0.149	-----	-----	-----	-----	-----	0.199	-----	-----	-----	-----	-----	0.253
1.50	.034						.099						.143
2.50	.020	0.012	0.021	0.069	0.144	0.210	.062	0.065	0.081	0.096	0.126	0.153	.094
3.50	.010						.039						.065
4.50	-.014	-.022	-.027	.007	.073	-----	.012	.014	.018	.057	.062	.087	.042
5.50	-.033						-.009						.014
6.50	-.059	-.072	-.078	-.058	.010	.073	-.037	-.036	-.050	-.013	.011	.031	-.011
8.50	-.060	-.078	-.094	-.070	-.009	.048	-.045	-.049	-.048	-.053	-.015	.001	-.020
10.50	-.063	-.084	-.105	-.090	-.037	.021	-.052	-.060	-.048	-.053	-.014	-.007	-.037
12.50	-.052	-.069	-.091	-.087	-.043	.012	-.045	-.049	-.051	-.043	-.032	-.015	-.053
14.50	-.069	-.087	-.117	-.115	-.071	-.022	-.067	-.073	-.076	-.076	-.062	-.052	-.065
16.50	-.049	-.079	-.097	-.102	-.063	-.013	-.049	-.056	-.061	-.060	-.048	-.034	-.047
17.17	-.043						-.046						-.047
18.17	-.033	-.052	-.083	-.096	-.062	-.014	-.037	-.044	-.051	-.053	-.044	-.032	-.040
19.17	-.015						-.018						-.020
20.17	-.015	-.026	-.056	-.070	-.037	.014	-.016	-.018	-.028	-.050	-.026	-.006	-.018
21.17	-.002		-.067	-.058	-.024		-.008		-.037	-.022	-.014		-.012
22.17	.003	-.020	-.044	-.050	-.020	.026	.000	-.011	-.016	-.013	-.010	.008	-.002
23.17	.007		-.042	-.048	-.018		.002		-.013	-.009	-.004		-.002
24.17	.009	-.016		-.047	-.015	.029	.004	-.004	-.012	-.008	-.002	.011	.002
25.17	.008		-.034	-.046	-.014		.004			-.008	-.002		.003
26.17		-.014		-.041		.028		-.003		-.005		.008	
27.17	.006			-.038	-.008		.004		-.016	-.009	.001		.005
28.17	.005	-.014		-.043		.031	.004	-.003		-.010		.011	.005
29.18	.003						.005						.002
30.17	.008	-.011		-.045	-.012	.032	.007	.001		-.009	-.002	.011	.007
31.17	.004			-.045	-.009		.013			-.007	.000		.002
32.17	.000	-.013		-.040	-.011	.031	.002	-.002		-.007	.000	.011	.002
33.17	.001						.003						.005
34.17	.003	-.012	-.023	-.041	-.012	.031	.003	-.002	-.006	-.008	-.001	.012	.004
35.17	.000						.001						.001
36.17	.000	-.016	-.028	-.043	-.010	.037	-.001	-.009	-.012	-.011	-.002	.014	.000
37.17	-.008						-.009						-.007
38.15	-.022	-.037	-.047	-.058	-.021	.017	-.024	-.032	-.032	-.029	-.016	-.006	-.024
38.40	-.025						-.030						-.033
38.65	-.035						-.042						-.047
38.90	-.050						-.056						-.074
39.15	-.105	-.095	-.140	-.179	-.145	-.095	-.089	-.085	-.125	-.132	-.146	-.132	-.117

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(g) M = 1.00

x, in.	Pressure coefficients of row –																	
	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°	θ = 0°	θ = 45°	θ = 75°	θ = 105°	θ = 135°	θ = 180°
	α = 20°						α = 16°						α = 12°					
0.50	0.078	—	—	—	—	—	0.106	—	—	—	—	—	0.129	—	—	—	—	—
1.50	.007	—	—	—	—	—	.057	—	—	—	—	—	.040	—	—	—	—	—
2.50	-.018	-0.125	-0.259	-0.138	0.154	0.442	.011	-0.078	-0.127	-0.026	0.180	0.369	.013	-0.050	-0.041	0.034	0.170	0.289
3.50	-.054	—	—	—	—	—	-.009	—	—	—	—	—	.012	—	—	—	—	—
4.50	-.046	-.131	-.314	-.219	.073	—	-.026	-.097	-.174	-.100	.093	—	-.018	-.059	-.088	-.028	.093	—
5.50	-.067	—	—	—	—	—	-.047	—	—	—	—	—	-.034	—	—	—	—	—
6.50	-.091	-.165	-.352	-.279	-.005	.270	-.066	-.132	-.227	-.168	.015	.205	-.063	-.107	-.141	-.080	.026	.138
8.50	-.078	-.168	-.353	-.317	-.052	.219	-.059	-.151	-.241	-.205	-.030	.156	-.056	-.107	-.158	-.119	-.011	.097
10.50	-.082	-.184	-.338	-.350	-.093	.183	-.070	-.142	-.253	-.233	-.069	.119	-.070	-.117	-.177	-.146	-.043	.065
12.50	-.080	-.181	-.893	-.565	-.117	.150	-.066	-.136	-.239	-.251	-.095	.071	-.061	-.106	-.173	-.158	-.065	.043
14.50	-.115	-.187	-.265	-.378	-.146	.106	-.095	-.149	-.241	-.272	-.123	.050	-.075	-.118	-.189	-.182	-.088	.007
16.50	-.112	-.176	-.225	-.372	-.160	.099	-.081	-.141	-.212	-.273	-.138	.040	-.064	-.115	-.176	-.154	-.097	.003
17.17	-.122	—	—	—	—	—	-.096	—	—	—	—	—	-.067	—	—	—	—	—
18.17	-.113	-.170	-.205	-.370	-.168	.080	-.091	-.136	-.194	-.273	-.152	.024	-.065	-.108	-.169	-.189	-.109	-.012
19.17	-.105	—	—	—	—	—	-.067	—	—	—	—	—	-.042	—	—	—	—	—
20.17	-.084	-.138	-.164	-.347	-.159	.088	-.052	-.111	-.147	-.250	-.138	.058	-.057	-.072	-.134	-.165	-.096	.000
21.17	-.027	—	-.140	-.323	-.149	—	-.070	—	-.145	-.220	-.123	—	.001	—	-.116	-.133	-.079	—
22.17	-.006	-.078	-.081	-.275	-.138	.105	-.023	-.075	-.110	-.199	-.106	.054	.020	-.021	-.059	-.081	-.059	.046
23.17	-.028	—	-.086	-.193	-.072	—	.001	—	-.062	-.179	-.092	—	.019	—	-.056	-.069	-.011	—
24.17	-.037	-.086	—	-.256	-.056	.161	.007	-.054	—	-.117	-.040	.099	.016	-.020	—	-.074	-.007	.077
25.17	-.028	—	—	-.218	-.070	—	.001	—	—	-.126	-.052	—	.007	—	-.050	-.077	-.014	—
26.17	—	.086	—	-.255	—	.148	—	-.058	—	-.128	—	.115	—	-.024	—	-.076	—	.066
27.17	-.036	—	-.103	-.251	-.072	—	-.006	—	-.061	-.151	-.051	—	-.004	—	—	-.072	-.014	—
28.17	-.026	-.084	-.096	-.244	—	.140	-.010	-.047	-.057	-.157	—	.107	-.008	-.030	—	-.100	—	.061
29.17	-.038	—	—	-.256	—	—	-.018	—	—	-.156	—	—	-.012	—	—	-.096	—	—
30.17	-.053	-.079	—	-.239	-.087	.137	-.016	-.044	—	-.151	-.053	.097	-.008	-.028	—	-.096	-.051	.058
31.17	-.032	—	-.087	-.235	-.078	—	-.012	—	-.062	-.152	-.051	—	-.004	—	—	-.091	-.025	—
32.17	-.044	-.080	-.085	-.232	-.067	.136	-.009	-.048	-.062	-.154	-.058	.089	-.013	-.032	—	-.093	-.052	.057
33.17	-.055	—	—	—	—	—	-.018	—	—	—	—	—	-.013	—	—	—	—	—
34.17	-.048	-.080	-.086	-.226	-.090	.138	-.012	-.047	-.058	-.153	-.065	.085	-.008	-.050	-.049	-.091	-.053	.057
35.17	-.055	—	—	—	—	—	-.018	—	—	—	—	—	-.014	—	—	—	—	—
36.17	-.054	-.082	-.087	-.230	-.080	.146	-.016	-.048	-.058	-.150	-.054	.095	-.011	-.054	-.054	-.092	-.026	.063
37.17	-.065	—	—	—	—	—	-.028	—	—	—	—	—	-.018	—	—	—	—	—
38.15	-.077	-.103	-.106	-.240	-.091	.126	-.042	-.067	-.070	-.155	-.059	.081	-.033	-.057	-.070	-.105	-.053	.048
38.40	-.083	—	—	—	—	—	-.045	—	—	—	—	—	-.058	—	—	—	—	—
38.65	-.095	—	—	—	—	—	-.061	—	—	—	—	—	-.056	—	—	—	—	—
38.90	-.109	—	—	—	—	—	-.082	—	—	—	—	—	-.076	—	—	—	—	—
39.15	-.145	-.214	-.220	-.347	-.201	.018	-.119	-.185	-.195	-.260	-.156	-.009	-.119	-.171	-.201	-.214	-.135	-.042
	α = 8°						α = 4°						α = 0°					
0.50	0.162	—	—	—	—	—	0.211	—	—	—	—	—	0.226					
1.50	.068	—	—	—	—	—	.108	—	—	—	—	—	.158					
2.50	.052	0.022	0.053	0.082	0.155	0.221	.072	0.076	0.090	0.106	0.138	0.164	.104					
3.50	.023	—	—	—	—	—	.046	—	—	—	—	—	.077					
4.50	-.002	-.013	-.016	.016	.083	—	.020	.022	.028	.046	.073	.097	.055					
5.50	-.024	—	—	—	—	—	-.005	—	—	—	—	—	.025					
6.50	-.051	-.065	-.072	-.058	.016	.078	-.034	-.035	-.027	-.008	.018	.058	-.006					
8.50	-.050	-.071	-.087	-.063	-.005	.051	-.058	-.041	-.042	-.027	-.009	.009	-.014					
10.50	-.071	-.093	-.109	-.092	-.040	.018	-.063	-.070	-.068	-.055	-.038	-.018	-.045					
12.50	-.067	-.086	-.109	-.102	-.055	.001	-.063	-.068	-.069	-.060	-.047	-.029	-.050					
14.50	-.079	-.100	-.127	-.125	-.079	-.050	-.060	-.064	-.088	-.082	-.069	-.057	-.069					
16.50	-.072	-.094	-.120	-.124	-.082	-.051	-.075	-.080	-.084	-.080	-.070	-.053	-.065					
17.17	-.073	—	—	—	—	—	-.077	—	—	—	—	—	-.070					
18.17	-.056	-.086	-.118	-.127	-.090	-.040	-.075	-.078	-.086	-.063	-.074	-.056	-.068					
19.17	-.043	—	—	—	—	—	-.057	—	—	—	—	—	-.051					
20.17	-.028	-.041	-.078	-.100	-.074	-.025	-.043	-.045	-.057	-.062	-.059	-.042	-.039					
21.17	.007	—	-.062	-.059	-.057	—	-.021	—	-.053	-.055	-.051	—	-.001					
22.17	.022	-.006	-.026	-.057	-.008	.040	.014	.004	-.001	.004	.006	.022	.020					
23.17	.024	—	-.025	-.030	.000	—	.020	—	.006	.013	.019	—	.021					
24.17	.024	-.004	—	-.051	-.001	.043	.019	.011	.005	.010	.016	.051	.017					
25.17	.019	—	-.024	-.055	-.005	—	.016	—	—	.007	.014	—	.013					
26.17	—	-.009	—	-.056	—	.054	.006	.005	—	.005	.008	.020	.006					
27.17	.012	—	—	-.051	-.005	—	.006	—	-.012	.001	—	—	.006					
28.17	.008	-.013	—	-.043	—	.050	.004	-.003	—	-.006	—	.016	.005					
29.17	.006	—	—	-.048	—	—	.001	—	—	-.009	—	—	.005					
30.17	.009	-.012	—	-.044	-.014	.051	.004	-.002	—	-.008	-.001	.013	.010					
31.17	.007	—	—	-.042	-.011	—	-.002	—	—	-.007	.000	—	.002					
32.17	.002	-.013	—	-.042	-.014	.029	-.002	-.005	—	-.007	.000	.012	.002					
33.17	.005	—	—	—	—	—	.000	—	—	—	—	—	.004					
34.17	.005	-.011	-.025	-.041	-.014	.028	.005	-.005	-.007	-.007	.001	.013	.007					
35.17	.000	—	—	—	—	—	.001	—	—	—	—	—	.002					
36.17	-.001	-.016	-.027	-.043	-.011	.035	-.001	-.007	-.011	-.009	.001	.016	.002					
37.17	-.010	—	—	—	—	—	-.008	—	—	—	—	—	-.005					
38.15	-.027	-.041	-.047	-.055	-.019	.020	-.028	-.035	-.053	-.025	-.010	.000	-.019					
38.40	-.035	—	—	—	—	—	-.037	—	—	—	—	—	-.029					
38.65	-.050	—	—	—	—	—	-.052	—	—	—	—	—	-.046					
38.90	-.071	—	—	—	—	—	-.078	—	—	—	—	—	-.079					
39.15	-.124	-.137	-.173	-.176	-.129	-.078	-.122	-.125	-.156	-.159	-.139	-.113	-.147					

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(b) M = 1.05

Pressure coefficients of row —

x, in.	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
			α = 20°						α = 16°						α = 12°			
0.50	0.110	-----	-----	-----	-----	-----	0.127	-----	-----	-----	-----	-----	0.158	-----	-----	-----	-----	-----
1.50	.041						.058						.072					
2.50	.017	-0.090	-0.218	-0.105	0.197	0.467	.040	-0.057	-0.106	0.000	0.200	0.388	.046	0.001	-0.009	0.065	0.197	0.316
3.50	.005						.021						.044					
4.50	-.012	-.095	-.274	-.179	.110	-----	.011	-.063	-.142	-.063	.119	-----	.015	-.023	-.052	.005	.122	-----
5.50	-.028						-.008						-.007					
6.50	-.053	-.124	-.305	-.236	.036	.302	-.029	-.094	-.186	-.127	.052	.233	-.027	-.070	-.104	-.049	.055	.166
8.50	-.051	-.135	-.316	-.275	-.014	.251	-.022	-.093	-.199	-.162	.008	.288	-.029	-.077	-.127	-.087	.021	.124
10.50	-.057	-.155	-.308	-.314	-.057	.214	-.040	-.107	-.214	-.194	-.051	.151	-.045	-.092	-.150	-.118	-.014	.095
12.50	-.065	-.160	-.273	-.335	-.085	.176	-.046	-.112	-.213	-.219	-.065	.118	-.044	-.089	-.155	-.138	-.040	.064
14.50	-.101	-.176	-.254	-.357	-.121	.127	-.081	-.133	-.225	-.250	-.101	.070	-.063	-.107	-.175	-.167	-.074	.025
16.50	-.121	-.173	-.226	-.365	-.144	.113	-.082	-.137	-.209	-.262	-.124	.055	-.059	-.108	-.171	-.176	-.090	.015
17.17	-.122						-.096						-.068					
18.17	-.125	-.176	-.217	-.371	-.162	.086	-.095	-.139	-.197	-.272	-.142	.050	-.070	-.110	-.171	-.186	-.105	-.007
19.17	-.125						-.088						-.057					
20.17	-.116	-.166	-.192	-.371	-.166	.086	-.084	-.129	-.173	-.267	-.146	.050	-.075	-.096	-.155	-.180	-.106	-.005
21.17	-.107	-----	-.191	-.355	-.183	-----	-.076	-----	-.176	-.252	-.138	-----	-.078	-----	-.160	-.169	-.094	-----
22.17	-.106	-.159	-.179	-.352	-.162	.083	-.071	-.119	-.156	-.242	-.135	.033	-.045	-.091	-.144	-.154	-.088	.005
23.17	-.094	-----	-.164	-.313	-.157	-----	-.078	-----	-.138	-.231	-.134	-----	-.043	-----	-.132	-.153	-.087	-----
24.17	-.085	-.143	-----	-.310	-.122	.087	-.067	-.107	-----	-.219	-.118	.038	-.041	-.076	-----	-.149	-.080	.012
25.17	-.073	-----	-----	-.311	-.138	-----	-.060	-----	-----	-.216	-.112	-----	-.045	-----	-.105	-.139	-.077	-----
26.17	-----	-.128	-----	-.285	-----	.099	-----	-.096	-----	-.199	-----	.049	-----	-.071	-----	-.132	-----	.014
27.17	-.064	-----	-.135	-.291	-.113	-----	-.060	-----	-.113	-.198	-.092	-----	-.035	-----	-----	-.122	-.063	-----
28.17	-.064	-.124	-.125	-.278	-----	.106	-.054	-.091	-.099	-.205	-----	.057	-.053	.062	-----	-.130	-----	.027
29.17	-.068	-----	-----	-.278	-----	-----	-.060	-----	-----	-.201	-----	-----	-.056	-----	-----	-.128	-----	-----
30.17	-.062	-.112	-----	-.267	-.124	.109	-.050	-.081	-----	-.191	-.098	.057	-.025	-.049	-----	-.122	-.059	.054
31.17	-.064	-----	-.111	-.253	-.104	-----	-.054	-----	-.087	-.180	-.085	-----	.000	-----	-----	-.111	-.050	-----
32.17	-.061	-.102	-.107	-.252	-.110	.112	-.058	-.075	-.081	-.178	-.087	.060	-.021	-.043	-----	-.107	-.050	.054
33.17	-.053						-.041						-.021					
34.17	-.053	-.090	-.095	-.239	-.107	.118	-.029	-.058	-.069	-.167	-.083	.067	-.003	-.027	-.044	-.094	-.042	.044
35.17	-.054						-.018						.016					
36.17	-.043	-.076	-.078	-.222	-.085	.138	.000	-.039	-.047	-.143	-.060	.087	.037	.004	-.009	-.055	-.005	.080
37.17	-.030						-.013						.055					
38.15	-.037	-.068	-.073	-.208	-.075	.134	-.011	-.041	-.046	-.131	-.044	.091	.018	-.008	-.018	-.050	.014	.093
38.40	-.053						-.015						.014					
38.65	-.033						-.023						-.005					
38.90	-.050						-.028						-.021					
39.15	-.056	-.135	-.136	-.287	-.159	.052	-.057	-.121	-.129	-.219	-.122	.022	-.062	-.113	-.140	-.161	-.085	.005

x, in.	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
			α = 8°						α = 4°						α = 0°			
0.50	0.186	-----	-----	-----	-----	-----	0.236	-----	-----	-----	-----	-----	0.288					
1.50	.091						.155						.180					
2.50	.058	0.050	0.058	0.105	0.179	0.242	.101	0.103	0.118	0.133	0.162	0.186	.131					
3.50	.052						.078						.107					
4.50	.033	.025	.019	.052	.115	-----	.057	.056	.060	.079	.102	.128	.085					
5.50	.015						.036						.059					
6.50	-.014	-.028	-.053	.001	.054	.112	.008	.006	.012	.051	.053	.070	.051					
8.50	-.018	-.057	-.052	-.027	.029	.083	-.005	-.009	-.008	.005	.024	.042	.019					
10.50	-.044	-.065	-.083	-.062	.012	.046	-.033	-.039	-.058	-.025	-.007	.012	-.018					
12.50	-.052	-.070	-.094	-.085	-.037	.021	-.043	-.048	-.050	-.042	-.026	-.009	-.038					
14.50	-.070	-.090	-.118	-.114	-.067	-.017	-.064	-.071	-.073	-.070	-.036	-.043	-.064					
16.50	-.070	-.091	-.117	-.119	-.078	-.026	-.066	-.075	-.079	-.076	-.063	-.048	-.065					
17.17	-.073						-.069						-.072					
18.17	-.072	-.090	-.120	-.127	-.089	-.040	-.071	-.076	-.083	-.085	-.073	-.058	-.072					
19.17	-.060						-.061						-.063					
20.17	-.063	-.074	-.108	-.119	-.086	-.054	-.060	-.063	-.074	-.076	-.069	-.050	-.062					
21.17	-.057	-----	-.114	-.100	-.075	-----	-.059	-----	-.082	-.060	-.057	-----	-.060					
22.17	-.046	-.072	-.099	-.103	-.067	-.020	-.049	-.064	-.068	-.064	-.054	-.037	-.050					
23.17	-.040	-----	-.095	-.098	-.071	-----	-.042	-----	-.059	-.055	-.051	-----	-.040					
24.17	-.035	-.059	-----	-.095	-.061	-.014	-.037	-.049	-.059	-.054	-.045	-.029	-.041					
25.17	-.031	-----	-.075	-.093	-.062	-----	-.033	-----	-----	-.051	-.045	-----	-.041					
26.17	-----	-.051	-----	-.080	-----	-.016	-----	-.036	-----	-.040	-----	-.032	-----					
27.17	-.022	-----	-.067	-.076	-.047	-----	-.031	-----	-.050	-.037	-.031	-----	-.029					
28.17	-.020	-.045	-----	-.076	-----	.003	-.028	-.037	-----	-.040	-----	-.019	-.021					
29.17	-.023	-----	-----	-.076	-----	-----	-.025	-----	-----	-.040	-----	-----	-.027					
30.17	-.015	-.038	-----	-.072	-.044	.006	-.014	-.023	-----	-.036	-.051	-.013	-.013					
31.17	-.015	-----	-----	-.062	-.035	-----	-.017	-----	-----	-.030	-.023	-----	-.020					
32.17	-.014	-.028	-----	-.058	-.034	.010	-.011	-.017	-----	-.023	-.020	-.010	-.014					
33.17	-.003						-.004						-.005					
34.17	.018	-.002	-.013	-.039	-.017	.022	.006	.000	-.005	-.008	-.005	.006	.014					
35.17	.050						.017						.033					
36.17	.040	.025	.015	-.002	.030	.073	.032	.023	.019	.021	.029	.039	.050					
37.17	.038						.036						.053					
38.15	.029	.012	.008	.000	.035	.073	.025	.018	.019	.027	.039	.046	.037					
38.40	.022						.017						.026					
38.65	.009						.005						.008					
38.90	-.010						-.017						-.024					
39.15	-.061	-.069	-.104	-.119	-.074	-.024	-.057	-.053	-.087	-.102	-.085	-.067	-.086					

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(1) M = 1.08

Pressure coefficients of row —

x, in.	α = 20° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 16° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 12° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
0.50	0.112	———	———	———	———	———	0.122	———	———	———	———	———	0.124	———	———	———	———	———
1.50	.045						.046						.063					
2.50	.001	-0.097	-0.228	-0.099	0.205	0.471	.017	-0.069	-0.104	0.000	0.202	0.384	.037	-0.004	-0.013	0.062	0.197	0.317
3.50	-.005						-.020						.049					
4.50	-.019	-.105	-.280	-.174	.113	———	.006	-.065	-.144	-.056	.125	———	.026	-.017	-.046	.009	.128	———
5.50	-.025						-.015						.000					
6.50	-.039	-.114	-.303	-.257	.059	.303	-.035	-.097	-.186	-.124	.056	.234	-.023	-.062	-.096	-.043	.060	.169
8.50	-.058	-.139	-.316	-.269	-.010	.253	-.034	-.107	-.225	-.177	.001	.184	-.051	-.078	-.126	-.084	.027	.128
10.50	-.089	-.175	-.326	-.318	-.055	.214	-.057	-.114	-.212	-.210	-.048	.137	-.052	-.085	-.152	-.117	-.009	.098
12.50	-.071	-.157	-.270	-.334	-.092	.172	-.048	-.108	-.202	-.205	-.055	.127	-.045	-.087	-.150	-.141	-.047	.063
14.50	-.065	-.156	-.207	-.363	-.114	.138	-.054	-.111	-.219	-.248	-.065	.089	-.077	-.115	-.178	-.164	-.068	.027
16.50	-.072	-.150	-.170	-.322	-.129	.125	-.044	-.102	-.160	-.248	-.111	.073	-.032	-.083	-.151	-.165	-.082	.016
17.17	-.072						-.052						-.057					
18.17	-.083	-.139	-.162	-.329	-.130	.117	-.051	-.100	-.146	-.229	-.115	.047	-.053	-.077	-.132	-.147	-.080	.023
19.17	-.087						-.046						-.016					
20.17	-.072	-.122	-.143	-.308	-.120	.125	-.044	-.089	-.119	-.220	-.108	.062	-.017	-.055	-.108	-.144	-.075	.027
21.17	-.067		-.144	-.294	-.112		-.045		-.123	-.205	-.100		-.028		-.109	-.122	-.064	
22.17	-.041	-.101	-.128	-.306	-.111	.124	-.040	-.085	-.111	-.192	-.094	.065	-.007	-.043	-.085	-.105	-.050	.037
23.17	-.039		-.109	-.266	-.111		-.038		-.099	-.182	-.089		.023		-.062	-.093	-.054	
24.17	-.059	-.094		-.255	-.096	.125	-.036	-.075		-.176	-.071	.076	.053	-.007		-.084	-.026	.055
25.17	-.065			-.249	-.096		-.039			-.181	-.074		.021		-.031	-.062	-.022	
26.17		-.104		-.241		.151		.002		-.156		.089		-.021		-.059		.064
27.17	-.060		-.110	-.249	-.079		.054		.001	-.062	.005		-.013			-.071	-.001	
28.17	-.056	-.100	-.098	-.242		.135	.013	-.012	.019	-.087		.163	-.025	-.041		-.095		.083
29.17	-.049			-.235			-.023			-.140			-.043			-.101		
30.17	-.010	-.061		-.205	-.053	.174	.054	-.055		-.157	-.046	.119	-.040	-.056		-.100	-.033	.050
31.17	-.019		-.071	-.207	-.017		.068		-.076	-.169	-.039		-.009			-.075	-.001	
32.17	-.058	-.068	-.076	-.234	-.052	.189	-.061	-.076	-.087	-.184	-.085	.072	-.015	-.022		-.074	.007	.108
33.17	-.049						-.068						-.011					
34.17	-.058	-.087	-.100	-.258	-.099	.145	-.065	-.080	-.094	-.188	-.098	.054	-.015	-.052	-.064	-.114	-.045	.056
35.17	-.070						-.062						-.029					
36.17	-.082	-.109	-.114	-.274	-.111	.128	-.069	-.088	-.097	-.193	-.095	.063	-.052	-.050	-.077	-.126	-.060	.038
37.17	-.092						-.071						-.045					
38.15	-.100	-.126	-.124	-.273	-.126	.097	-.073	-.096	-.101	-.196	-.101	.042	-.048	-.071	-.086	-.139	-.073	.008
38.40	-.099						-.075						-.048					
38.65	-.103						-.079						-.052					
38.90	-.111						-.081						-.062					
39.15	-.124	-.226	-.252	-.314	-.171	.060	-.098	-.204	-.209	-.243	-.143	.007	-.088	-.184	-.189	-.185	-.115	-.025

x, in.	α = 8° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 4° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	α = 0° θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
0.50	0.152	———	———	———	———	———	0.206	———	———	———	———	———	0.246					
1.50	.082						.107						.169					
2.50	.048	0.039	0.046	0.095	0.173	0.241	.082	0.066	0.100	0.114	0.149	0.177	.111					
3.50	.051						.081						.090					
4.50	.031	.020	.012	.051	.112	———	.058	.056	.060	.077	.099	.124	.074					
5.50	.004						.033						.051					
6.50	-.017	-.050	-.059	-.009	.050	.108	.007	.006	.013	.050	.050	.067	.026					
8.50	-.025	-.043	-.059	-.056	.018	.074	-.009	-.015	-.015	.001	.016	.052	.012					
10.50	-.040	-.059	-.073	-.057	-.006	.047	-.028	-.034	-.054	-.021	-.006	.009	-.009					
12.50	-.055	-.079	-.106	-.094	-.038	.024	-.041	-.050	-.055	-.059	-.018	.005	-.018					
14.50	-.065	-.080	-.107	-.110	-.071	-.020	-.054	-.060	-.069	-.072	-.062	-.045	-.062					
16.50	-.056	-.073	-.094	-.091	-.047	-.004	-.066	-.070	-.069	-.065	-.056	-.039	-.029					
17.17	-.058						-.066						-.027					
18.17	-.042	-.065	-.107	-.106	-.061	-.004	-.056	-.064	-.068	-.057	-.056	-.016	-.057					
19.17	-.024						-.023						-.042					
20.17	-.026	-.056	-.070	-.091	-.065	-.009	-.021	-.026	-.040	-.050	-.053	-.051	-.046					
21.17	-.017		-.073	-.066	-.047		-.020		-.044	-.027	-.051		-.017					
22.17	-.004	-.051	-.059	-.067	-.037	.004	-.011	-.020	-.024	-.019	-.011	-.001	-.008					
23.17	.004		-.052	-.060	-.037		.001		-.015	-.013	-.011		-.001					
24.17	.008	-.020		-.056	-.029	.014	.008	-.002	-.015	-.013	-.009	.003	-.002					
25.17	.010		-.055	-.052	-.024		.016			-.009	-.005		.005					
26.17		-.007		-.039		.018		.024		.008		.006						
27.17	.035			-.023	-.005		.041		.013	.017	.019		.031					
28.17	.044	.019		-.006		.068	.023	.016		.017		.056	.041					
29.17	.058			.002			.010			.040			.039					
30.17	.051	.009		-.006	.036	.086	.019	.014		.028	.050	.081	.061					
31.17	.011			-.030	.009		.014			.006	.021		.017					
32.17	-.011	-.023		-.051	.018	.051	.004	-.002		-.010	-.005	.009	-.006					
33.17	-.023						-.005						-.021					
34.17	-.023	-.039	-.054	-.076	-.047	-.003	-.012	-.021	-.051	-.057	-.054	-.022	-.026					
35.17	-.035						-.024						-.035					
36.17	-.035	-.049	-.063	-.083	-.050	.000	-.028	-.034	-.059	-.042	-.056	-.021	-.032					
37.17	-.041						-.054						-.034					
38.15	-.048	-.062	-.072	-.089	-.054	-.017	-.042	-.051	-.052	-.051	-.040	-.052	-.037					
38.40	-.043						-.050						-.059					
38.65	-.057						-.062						-.049					
38.90	-.073						-.068						-.072					
39.15	-.105	-.172	-.176	-.152	-.109	-.058	-.146	-.156	-.158	-.134	-.111	-.091	-.148					

TABLE I.- Continued

PRESSURE DATA, CYLINDRICAL BODY

(j) M = 1.10

Pressure coefficients of row –

x, in.	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
	α = 20°						α = 16°						α = 12°					
0.50	0.097	----	----	----	----	----	0.119	----	----	----	----	----	0.117	----	----	----	----	----
1.50	.058	----	----	----	----	----	.051	----	----	----	----	----	.045	----	----	----	----	----
2.50	.006	-0.092	-0.227	-0.089	0.215	0.476	.020	-0.068	-0.098	0.001	0.205	0.390	.010	-0.023	-0.051	0.045	0.175	0.290
3.50	.008	----	----	----	----	----	.024	----	----	----	----	----	.041	----	----	----	----	----
4.50	-.012	-.097	-.261	-.161	.123	----	.008	-.062	-.142	-.066	.123	----	.025	-.017	-.045	.006	.123	----
5.50	-.058	----	----	----	----	----	-.014	----	----	----	----	----	.002	----	----	----	----	----
6.50	-.058	-.131	-.310	-.227	.051	.311	-.051	-.095	-.187	-.127	.055	.234	-.017	-.057	-.093	-.041	.066	.177
8.50	-.042	-.131	-.307	-.271	.002	.260	-.029	-.094	-.201	-.161	.011	.187	-.025	-.069	-.118	-.079	.027	.129
10.50	-.074	-.160	-.307	-.307	-.048	.218	-.043	-.119	-.233	-.198	-.022	.157	-.048	-.089	-.146	-.112	-.010	.096
12.50	-.090	-.172	-.289	-.332	-.075	.181	-.053	-.112	-.217	-.246	-.077	.110	-.027	-.078	-.135	-.131	-.028	.074
14.50	-.091	-.167	-.246	-.375	-.117	.133	-.085	-.140	-.221	-.245	-.110	.082	-.058	-.096	-.150	-.159	-.071	.055
16.50	-.093	-.160	-.185	-.374	-.159	.119	-.065	-.122	-.193	-.233	-.097	.065	-.069	-.111	-.170	-.168	-.077	.021
17.17	-.090	----	----	----	----	----	-.068	----	----	----	----	----	-.054	----	----	----	----	----
18.17	-.090	-.155	-.163	-.314	-.153	.096	-.056	-.104	-.166	-.256	-.110	.066	-.049	-.092	-.165	-.186	-.102	.000
19.17	-.090	----	----	----	----	----	-.049	----	----	----	----	----	-.037	----	----	----	----	----
20.17	-.071	-.138	-.145	-.315	-.118	.112	-.045	-.090	-.125	-.235	-.129	.051	-.024	-.070	-.121	-.139	-.103	.001
21.17	-.089	----	-.145	-.302	-.114	----	-.047	----	-.124	-.210	-.114	----	-.032	----	-.119	-.132	-.082	----
22.17	-.079	-.123	-.138	-.313	-.118	.119	-.048	-.083	-.105	-.200	-.094	.059	-.022	-.063	-.104	-.120	-.065	.015
23.17	-.067	----	-.127	-.267	-.116	----	-.035	----	-.087	-.177	-.088	----	-.014	----	-.054	-.113	-.048	----
24.17	-.069	-.110	----	-.263	-.099	.123	-.028	-.069	----	-.171	-.069	.077	-.014	-.049	----	-.111	-.041	.046
25.17	-.044	----	----	-.269	-.087	----	-.038	----	----	-.178	-.076	----	-.016	----	-.071	-.111	-.044	----
26.17	----	-.080	----	-.258	----	.132	----	-.067	----	-.167	----	.076	----	-.043	----	-.101	----	.040
27.17	-.089	----	-.095	-.258	-.086	----	-.040	----	-.087	-.158	-.064	----	-.051	----	----	-.095	-.052	----
28.17	-.027	-.075	-.082	-.236	----	.127	-.059	-.071	-.083	-.173	----	.080	.034	-.024	----	-.102	----	.052
29.17	-.054	----	----	-.246	----	----	-.040	----	----	-.179	----	----	.015	----	----	-.089	----	----
30.17	-.047	-.077	----	-.219	-.097	.122	-.051	-.055	----	-.181	-.079	.074	.009	-.005	----	-.089	-.028	.052
31.17	-.042	----	-.067	-.187	-.081	----	-.008	----	-.045	-.163	-.074	----	.013	----	----	-.061	-.027	----
32.17	-.052	-.083	-.072	-.177	-.059	.123	.033	.016	.005	-.133	-.068	.074	-.011	-.019	----	-.056	-.006	.033
33.17	-.066	----	----	----	----	----	.045	----	----	----	----	----	-.016	----	----	----	----	----
34.17	-.061	-.065	-.066	-.213	-.059	.164	.054	.005	.004	-.064	.060	.202	-.019	-.050	-.043	-.083	-.016	.080
35.17	-.028	----	----	----	----	----	-.006	----	----	----	----	----	-.017	----	----	----	----	----
36.17	-.013	-.057	-.052	-.179	----	.224	-.024	-.059	-.044	-.156	-.026	.159	-.023	-.026	-.042	-.074	-.004	.087
37.17	-.056	----	----	----	----	----	-.046	----	----	----	----	----	-.018	----	----	----	----	----
38.15	-.059	-.065	-.080	-.238	-.063	.164	-.057	-.065	-.077	-.174	-.075	.070	-.009	-.028	-.050	-.087	-.007	.088
38.40	-.058	----	----	----	----	----	-.057	----	----	----	----	----	-.011	----	----	----	----	----
38.65	-.064	----	----	----	----	----	-.062	----	----	----	----	----	-.019	----	----	----	----	----
38.90	-.075	----	----	----	----	----	-.066	----	----	----	----	----	-.031	----	----	----	----	----
39.15	-.094	-.181	-.200	-.290	-.132	.099	-.079	-.174	-.188	-.220	-.122	.028	-.057	-.149	-.161	-.156	-.074	.026

x, in.	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
	α = 8°						α = 4°						α = 0°					
0.50	0.154	----	----	----	----	----	0.199	----	----	----	----	----	0.233	----	----	----	----	----
1.50	.066	----	----	----	----	----	.112	----	----	----	----	----	.156	----	----	----	----	----
2.50	.013	0.010	0.024	0.078	0.158	0.226	.049	0.065	0.081	0.099	0.152	0.161	.092	----	----	----	----	----
3.50	.045	----	----	----	----	----	.045	----	----	----	----	----	.114	----	----	----	----	----
4.50	.038	.027	.017	.054	.114	----	.061	.052	.053	.072	.096	.131	.083	----	----	----	----	----
5.50	.012	----	----	----	----	----	.058	----	----	----	----	----	.046	----	----	----	----	----
6.50	-.007	-.022	-.033	-.001	.059	.113	.013	.015	.020	.037	.057	.075	.022	----	----	----	----	----
8.50	-.022	-.040	-.057	-.035	.020	.077	-.005	-.010	-.009	.001	.019	.058	.013	----	----	----	----	----
10.50	-.040	-.059	-.078	-.058	-.009	.046	-.029	-.034	-.033	-.024	-.010	.009	.014	----	----	----	----	----
12.50	-.036	-.051	-.073	-.065	.025	.029	-.035	-.058	-.038	-.033	-.020	-.002	-.022	----	----	----	----	----
14.50	-.063	-.086	-.114	-.101	.045	.013	-.049	-.060	-.063	-.054	-.031	.016	-.022	----	----	----	----	----
16.50	-.053	-.073	-.102	-.113	-.076	-.020	-.050	-.056	-.066	-.074	-.061	-.040	-.061	----	----	----	----	----
17.17	-.062	----	----	----	----	----	-.057	----	----	----	----	----	-.071	----	----	----	----	----
18.17	-.067	-.082	-.111	-.115	-.085	-.056	-.068	-.071	-.072	-.074	-.067	-.055	-.063	----	----	----	----	----
19.17	-.057	----	----	----	----	----	-.066	----	----	----	----	----	-.046	----	----	----	----	----
20.17	-.060	-.067	-.104	-.103	-.065	-.017	-.059	-.063	-.070	-.063	-.052	-.039	-.044	----	----	----	----	----
21.17	-.029	----	-.099	-.089	-.056	----	-.037	----	-.070	-.051	-.045	----	-.041	----	----	----	----	----
22.17	-.012	-.041	-.069	-.082	.048	.002	-.024	-.051	-.057	-.043	-.055	-.020	-.041	----	----	----	----	----
23.17	-.001	----	-.057	-.063	.047	----	-.010	----	-.026	-.025	-.025	----	-.015	----	----	----	----	----
24.17	.003	-.027	----	-.060	-.035	.003	-.004	-.013	-.022	-.019	-.015	-.001	.001	----	----	----	----	----
25.17	.001	----	-.047	-.060	-.029	----	-.004	----	-.021	-.013	----	----	-.001	----	----	----	----	----
26.17	----	-.022	----	-.045	----	.024	----	-.008	----	-.017	----	.001	----	----	----	----	----	----
27.17	.008	----	----	-.051	.008	----	-.007	----	-.015	-.005	.000	----	.002	----	----	----	----	----
28.17	.005	-.017	----	-.042	----	.053	-.006	-.009	----	-.008	----	.018	.006	----	----	----	----	----
29.17	-.001	----	----	-.047	----	----	-.007	----	----	-.005	----	----	.001	----	----	----	----	----
30.17	-.005	-.024	----	-.051	.019	.027	.001	-.004	----	-.009	-.001	.015	.006	----	----	----	----	----
31.17	-.002	----	----	-.052	-.020	----	.013	----	----	-.013	-.005	----	.000	----	----	----	----	----
32.17	.024	.003	----	-.054	-.025	.019	.052	.046	----	-.002	-.007	.004	.005	----	----	----	----	----
33.17	.059	----	----	----	----	----	.043	----	----	----	----	----	.056	----	----	----	----	----
34.17	.067	.042	.059	.042	.047	.068	.052	.025	.026	.032	.045	.063	.070	----	----	----	----	----
35.17	.049	----	----	----	----	----	.025	----	----	----	----	----	.064	----	----	----	----	----
36.17	.032	.016	.006	.000	.042	.103	.021	.018	.021	.030	.048	.070	.032	----	----	----	----	----
37.17	.007	----	----	----	----	----	.011	----	----	----	----	----	.005	----	----	----	----	----
38.15	-.012	-.026	-.035	-.049	-.017	.025	-.009	-.016	-.017	-.020	-.009	-.002	-.004	----	----	----	----	----
38.40	-.016	----	----	----	----	----	-.018	----	----	----	----	----	-.019	----	----	----	----	----
38.65	-.028	----	----	----	----	----	-.033	----	----	----	----	----	-.050	----	----	----	----	----
38.90	-.046	----	----	----	----	----	-.058	----	----	----	----	----	-.053	----	----	----	----	----
39.15	-.079	-.150	-.146	-.117	-.074	-.028	-.123	-.133	-.131	-.109	-.085	-.065	-.130	----	----	----	----	----

TABLE I.- Concluded

PRESSURE DATA, CYLINDIRCAL BODY

(k) M = 1.13

x, in.	\(\alpha = 20° \) θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	\(\alpha = 16° \) θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	\(\alpha = 12° \) θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
0.50	0.079	—	—	—	—	—	0.078	—	—	—	—	—	0.116	—	—	—	—	—
1.50	.023	—	—	—	—	—	.053	—	—	—	—	—	.057	—	—	—	—	—
2.50	.008	-0.096	-0.225	-0.080	0.219	0.473	.008	-0.081	-0.104	0.002	0.209	0.383	.019	-0.018	-0.026	0.050	0.182	0.300
3.50	.012	—	—	—	—	—	.029	—	—	—	—	—	.029	—	—	—	—	—
4.50	.005	-.085	-.250	-.147	.136	—	.013	-.056	-.133	-.053	.138	—	.013	-.018	-.040	.005	.121	—
5.50	-.016	—	—	—	—	—	.004	—	—	—	—	—	.002	—	—	—	—	—
6.50	-.041	-.111	-.280	-.206	.069	.324	-.019	-.085	-.174	-.109	.077	.251	-.011	-.053	-.092	-.040	.069	.280
8.50	-.053	-.134	-.308	-.244	.021	.274	-.018	-.085	-.194	-.147	.050	.200	-.015	-.058	-.109	-.073	.033	.138
10.50	-.056	-.135	-.289	-.294	-.024	.251	-.054	-.097	-.208	-.182	-.012	.160	-.027	-.068	-.126	-.099	.002	.109
12.50	-.070	-.154	-.848	-.332	-.061	.196	-.059	-.097	-.188	-.196	-.040	.129	-.057	-.073	-.132	-.112	-.017	.087
14.50	-.099	-.170	-.238	-.336	-.106	.145	-.058	-.122	-.232	-.252	-.065	.105	-.052	-.078	-.150	-.131	-.043	.051
16.50	-.087	-.156	-.211	-.349	-.117	.129	-.072	-.117	-.179	-.265	-.109	.068	-.055	-.080	-.146	-.168	-.068	.046
17.17	-.092	—	—	—	—	—	-.081	—	—	—	—	—	-.050	—	—	—	—	—
18.17	-.094	-.146	-.173	-.368	-.136	.109	-.089	-.122	-.169	-.251	-.152	.041	-.065	-.095	-.147	-.154	-.089	.012
19.17	-.094	—	—	—	—	—	-.081	—	—	—	—	—	-.060	—	—	—	—	—
20.17	-.084	-.150	-.150	-.344	-.147	.105	-.066	-.115	-.161	-.228	-.106	.050	-.026	-.077	-.145	-.175	-.090	.009
21.17	-.095	—	-.148	-.308	-.147	—	-.068	—	-.161	-.255	-.100	—	-.025	—	-.128	-.154	-.090	—
22.17	-.095	-.143	-.159	-.320	-.144	.087	-.066	-.102	-.142	-.250	-.107	.055	-.027	-.069	-.112	-.145	-.076	.013
23.17	-.069	—	-.126	-.268	-.124	—	-.050	—	-.117	-.219	-.113	—	-.019	—	-.099	-.130	-.075	—
24.17	-.061	-.117	—	-.261	-.109	.105	-.042	-.082	—	-.201	-.095	.053	-.021	-.057	—	-.128	-.065	.014
25.17	-.071	—	—	-.263	-.085	—	-.041	—	—	-.189	-.093	—	-.027	—	-.080	-.129	-.068	—
26.17	—	-.104	—	-.251	—	.125	—	-.074	-.086	-.175	—	.062	—	-.051	—	-.114	—	.025
27.17	-.063	-.113	-.255		-.080		-.029			-.179	-.072		-.050			-.107	-.047	
28.17	-.058	-.102	-.111	-.248		.125	-.056	-.071	-.077	-.167		.068	-.025	-.047		-.107		.037
29.17	-.058			-.263			-.041			-.166			-.040			-.102		
30.17	-.063	-.090		-.250	-.087	.125	-.040	-.065		-.155	-.057	.088	-.036	-.050		-.102	-.034	.045
31.17	-.050		-.096	-.253	-.078		-.050		-.068	-.151	-.041		-.061			-.102	-.028	
32.17	-.055	-.085	-.093	-.259	-.080	.139	-.046	-.087	-.072	-.157	-.056	.094	-.017	-.047		-.109	-.042	.051
33.17	-.043						-.041						-.039					
34.17	-.043	-.074	-.081	-.243	-.100	.126	-.046	-.066	-.062	-.178	-.071	.076	-.018	-.055	-.060	-.118	-.041	.052
35.17	-.043						-.044						-.007					
36.17	-.028	-.057	-.058	-.213	-.091	.127	-.051	-.062	-.082	-.180	-.081	.075	.005	-.012	-.053	-.095	-.057	.059
37.17	-.034						-.056						.005					
38.15	-.056	-.061	-.044	-.175	-.062	.121	-.055	-.065	-.069	-.161	-.082	.062	.012	-.015	-.020	-.053	-.038	.054
38.40	-.056						-.054						.022					
38.65	-.057						-.055						.017					
38.90	-.061						-.054						-.001					
39.15	-.075	-.160	-.149	-.195	-.098	.102	-.057	-.154	-.160	-.188	-.102	.037	-.026	-.123	-.127	-.114	-.058	.013

x, in.	\(\alpha = 8° \) θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	\(\alpha = 4° \) θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°	\(\alpha = 0° \) θ=0°	θ=45°	θ=75°	θ=105°	θ=135°	θ=180°
0.50	0.149	—	—	—	—	—	0.205	—	—	—	—	—	0.291					
1.50	.089	—	—	—	—	—	.122	—	—	—	—	—	.182					
2.50	.058	0.052	0.045	0.094	0.170	0.240	.079	0.088	0.105	0.115	0.145	0.172	.106					
3.50	.054	—	—	—	—	—	.069	—	—	—	—	—	.088					
4.50	.012	.012	.011	.055	.118	—	.042	.042	.048	.068	.095	.122	.067					
5.50	.013	—	—	—	—	—	.014	—	—	—	—	—	.065					
6.50	-.005	-.016	-.052	-.002	.099	.119	.016	.007	.008	.024	.044	.078	.046					
8.50	-.013	-.051	-.049	-.022	.052	.088	.005	-.001	-.001	.014	.051	.050	.015					
10.50	-.025	-.046	-.067	-.048	.002	.059	-.016	-.022	-.022	-.009	.009	.051	.000					
12.50	-.050	-.048	-.073	-.063	-.019	.054	-.020	-.025	-.029	-.025	-.013	.005	-.013					
14.50	-.039	-.053	-.082	-.078	-.056	.009	-.054	-.040	-.043	-.040	-.027	-.017	-.027					
16.50	-.045	-.074	-.099	-.088	-.056	.010	-.037	-.047	-.047	-.057	-.020	-.017	-.025					
17.17	-.056	—	—	—	—	—	-.043	—	—	—	—	—	-.018					
18.17	-.052	-.069	-.113	-.117	-.071	-.016	-.046	-.062	-.077	-.073	-.051	-.020	-.044					
19.17	-.058	—	—	—	—	—	-.057	—	—	—	—	—	-.056					
20.17	-.049	-.057	-.090	-.106	-.081	-.051	-.046	-.045	-.051	-.056	-.055	-.046	-.061					
21.17	-.041	—	-.087	-.073	-.062	—	-.051	—	-.062	-.050	-.050	—	-.044					
22.17	-.042	-.067	-.091	-.077	-.045	-.008	-.046	-.057	-.055	-.041	-.028	-.026	-.024					
23.17	-.022	—	-.093	-.088	-.050	—	-.027	—	-.057	-.046	-.033	—	-.025					
24.17	-.016	-.043	—	-.091	-.053	-.003	-.017	-.028	-.047	-.049	-.059	-.019	-.034					
25.17	-.013	—	-.061	-.084	-.056	—	-.019	—	—	-.059	-.040	—	-.042					
26.17	—	-.052	—	-.060	—	-.009	—	-.022	—	-.030	—	-.026	—					
27.17	-.004			-.050	-.030		-.013		-.004	-.017	-.018		-.007					
28.17	-.001	-.026		-.057		.014	-.009	-.014		-.019		.005	-.002					
29.17	-.002			-.052			-.008			-.016			-.004					
30.17	-.001	-.024		-.053	-.027	.013	-.004	-.009		-.012	-.006	.009	.002					
31.17	-.005			-.047	-.018		-.009			-.014	-.006		.000					
32.17	-.012	-.024		-.041	-.011	.052	-.013	-.017		-.017	-.008	.008	-.002					
33.17	-.017						-.017						-.002					
34.17	-.019	-.050	-.040	-.047	-.012	.054	-.013	-.024	-.027	-.022	-.004	.015	.002					
35.17	-.009						-.009						-.010					
36.17	-.014	-.025	-.043	-.065	-.052	.021	-.010	-.012	-.014	-.018	-.010	.007	-.018					
37.17	-.018						-.008						-.001					
38.15	-.011	-.025	-.058	-.061	-.040	-.005	.025	.015	.004	-.006	-.011	-.011	.012					
38.40	-.005						.054						.013					
38.65	-.007						.029						.010					
38.90	-.011						.009						-.009					
39.15	-.026	-.079	-.105	-.101	-.067	-.024	-.045	-.054	-.066	-.061	-.060	-.052	-.081					

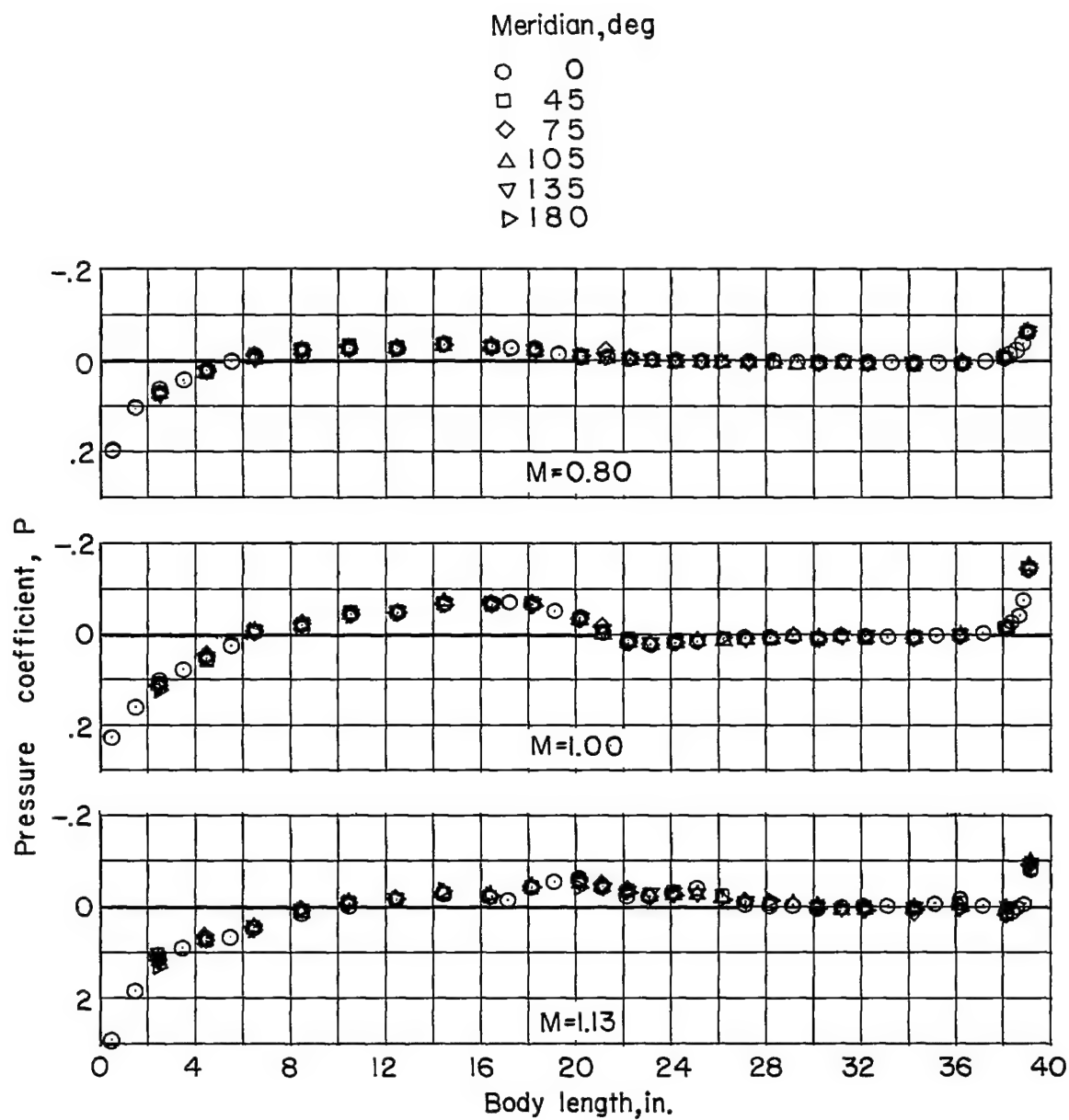Figure 1.- Body details. (Linear dimensions in inches.)

Meridian,deg

○ 0
□ 45
◇ 75
△ 105
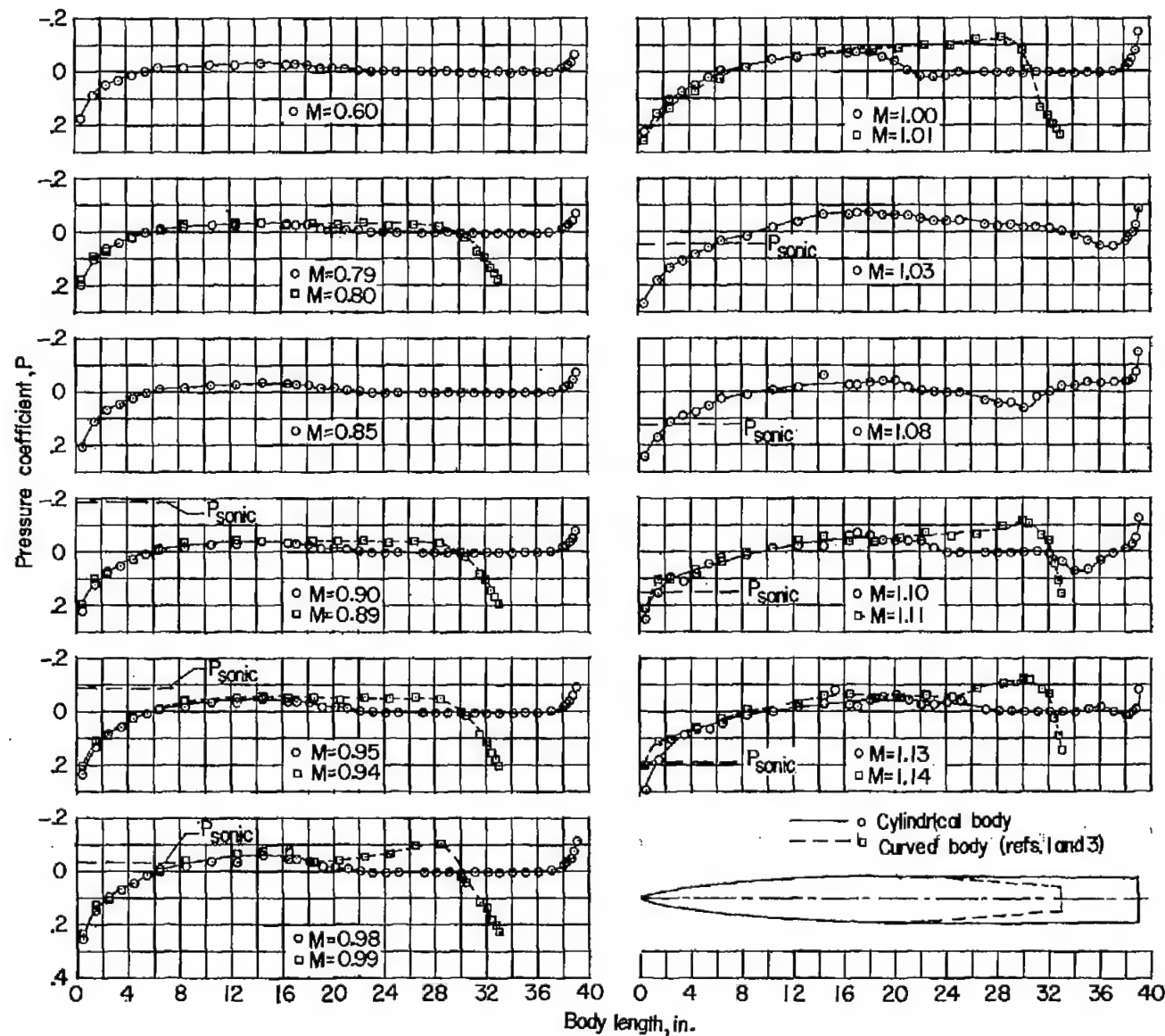▽ 135
▷ 180

Figure 2.- Accuracy of pressure measurements. α = 0°.

Figure 3.- Longitudinal pressure distribution at zero angle of attack.
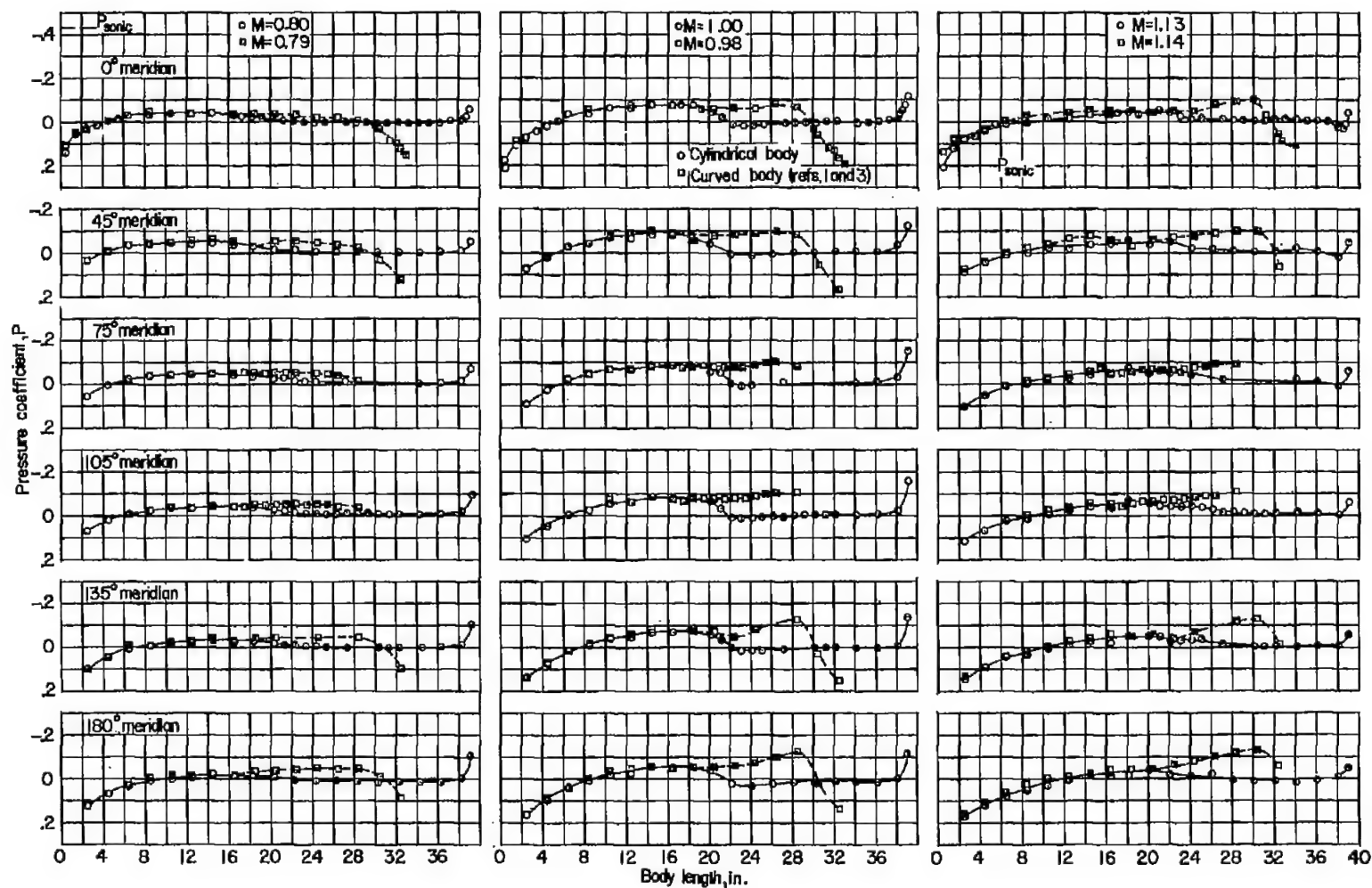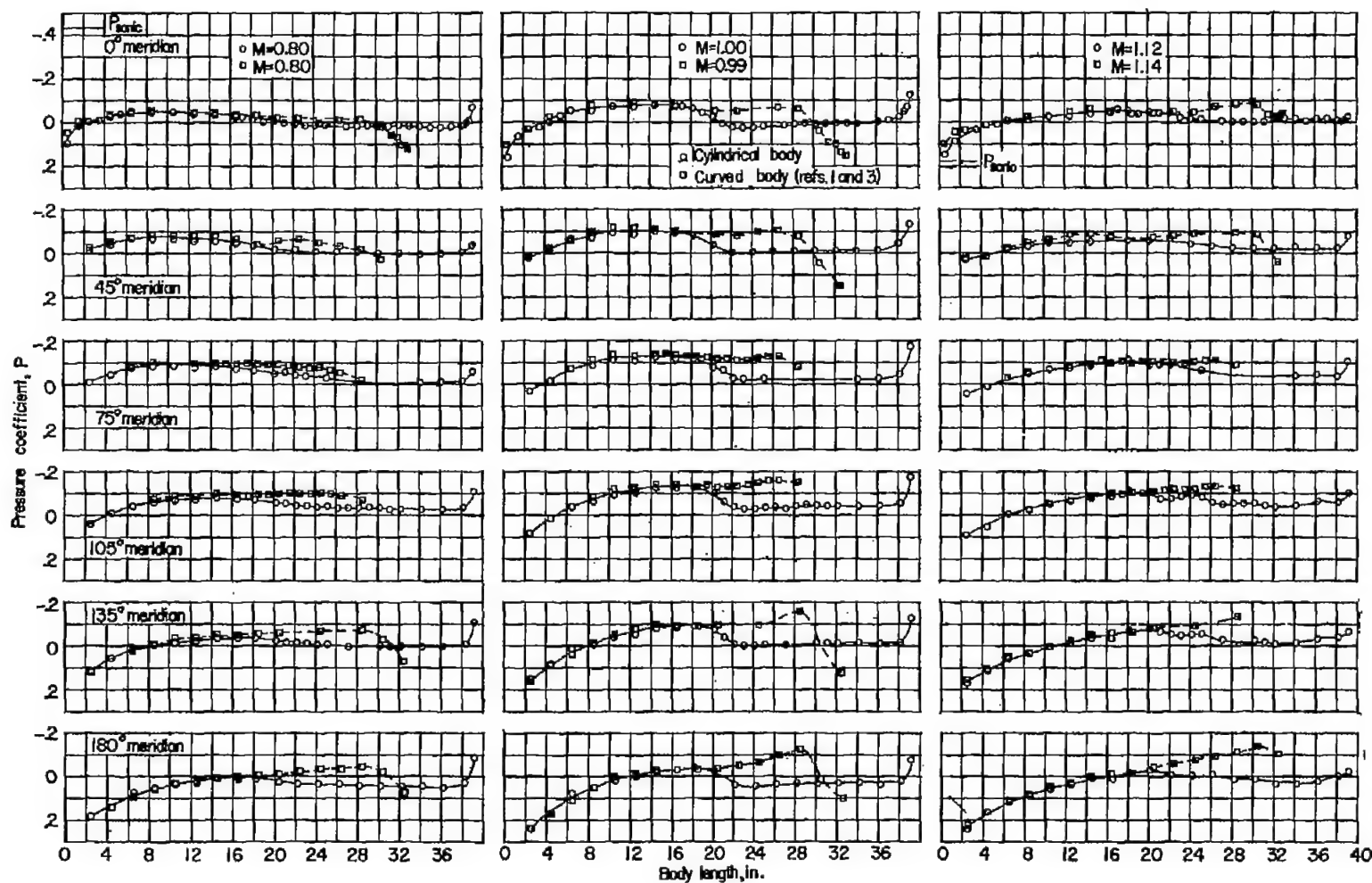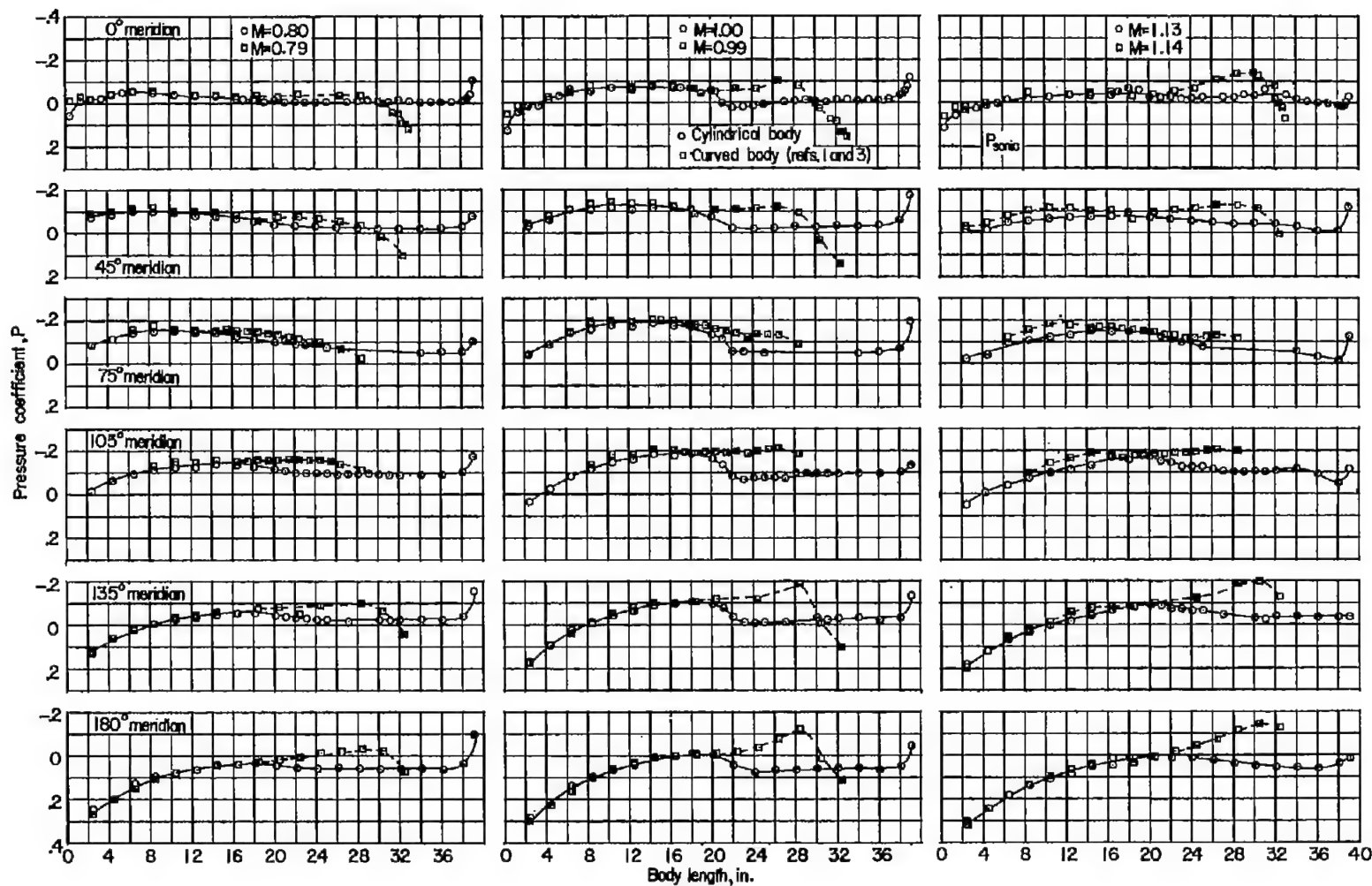
(a) α = 4°.

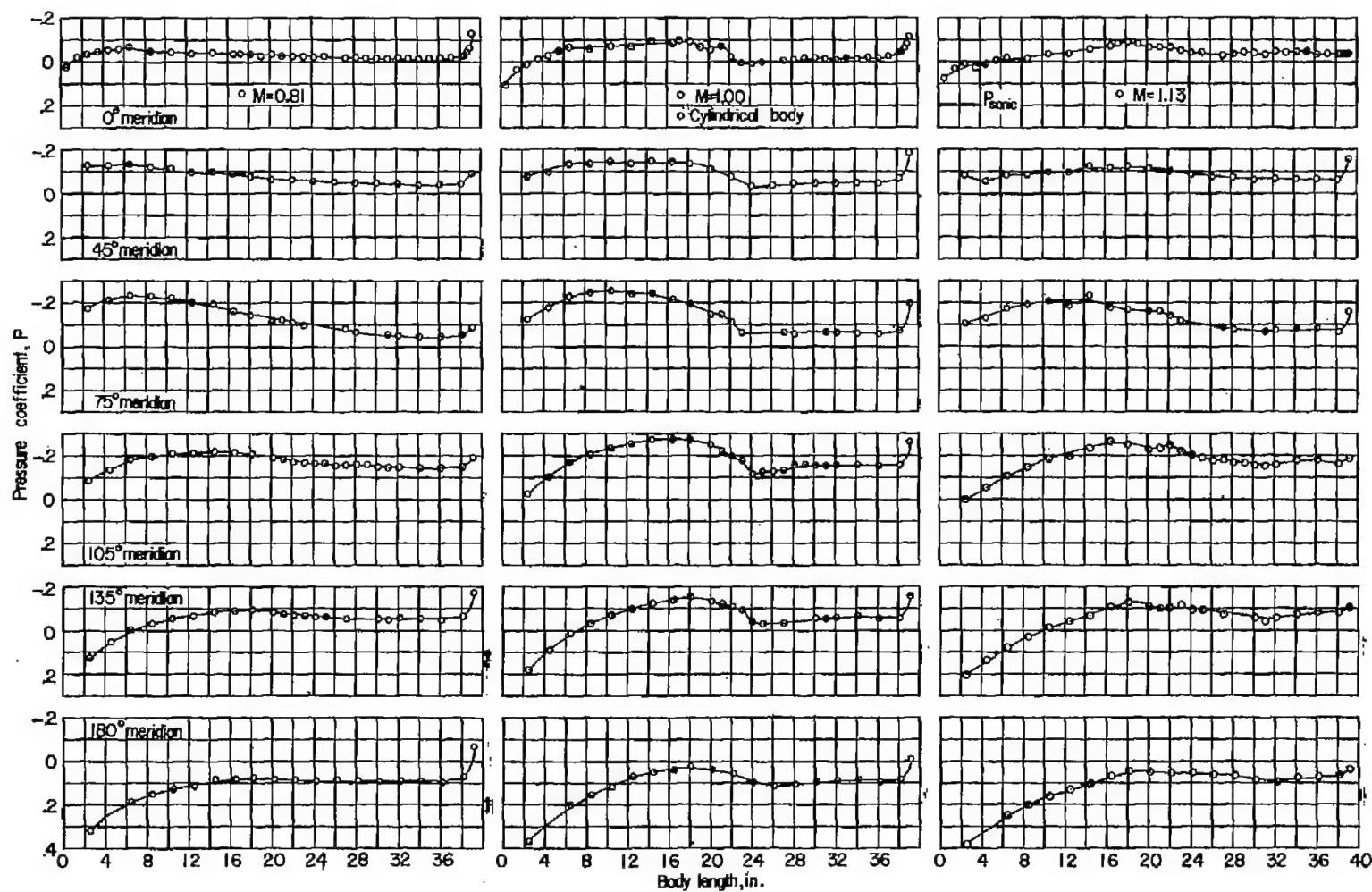Figure 4.- Longitudinal pressure distribution at six radial stations.
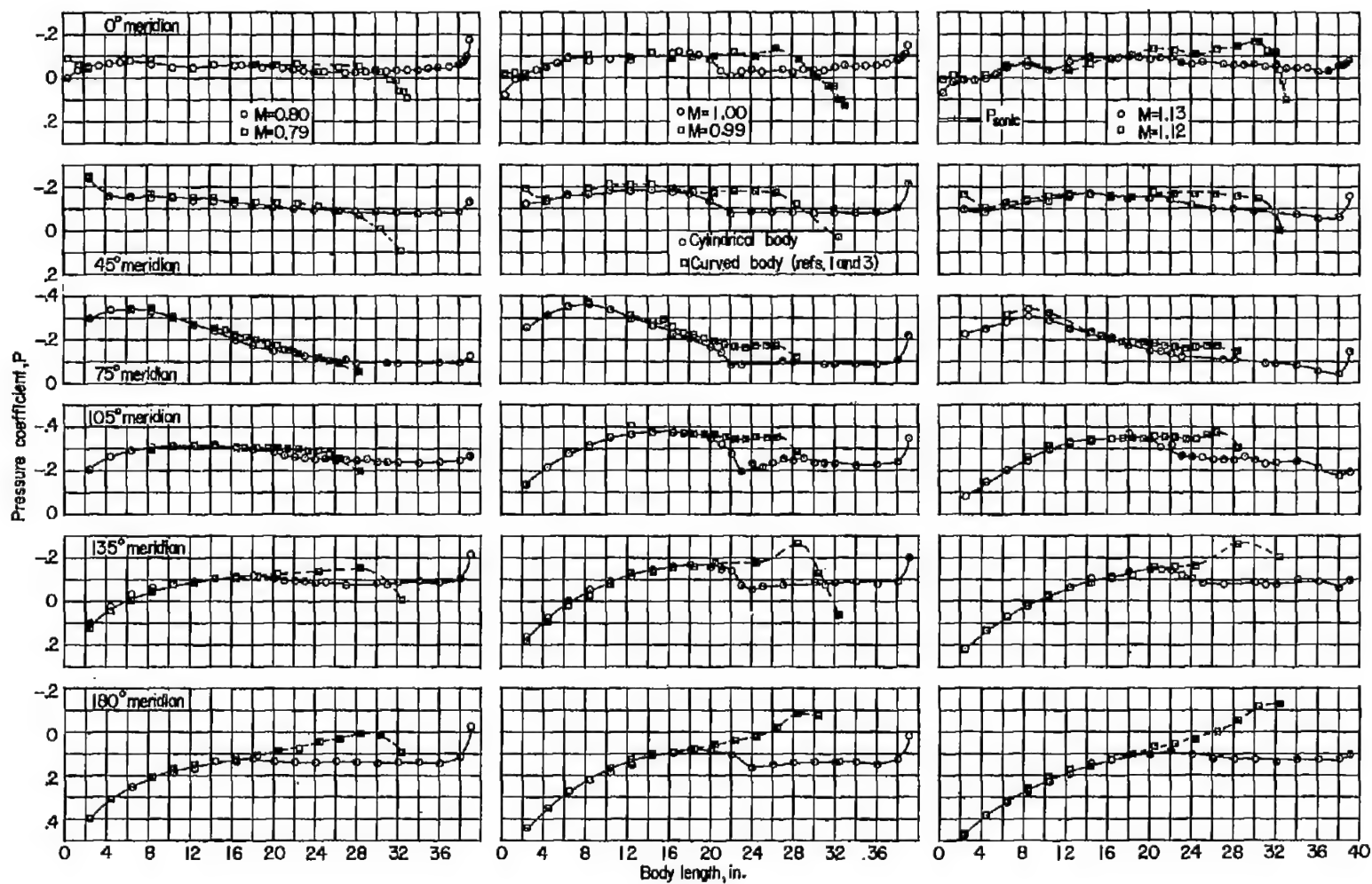
(b) $\alpha = 8^{o}$.

Figure 4.- Continued.
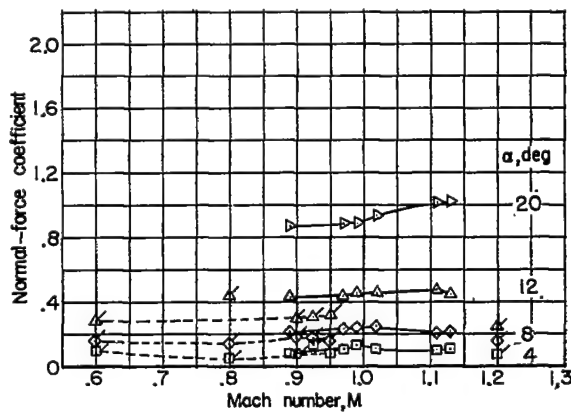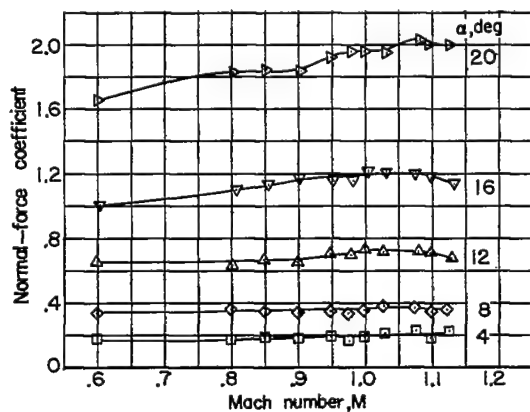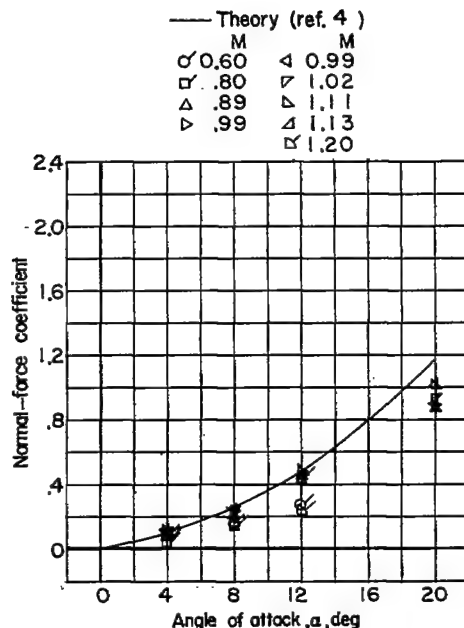
(c) $\alpha = 12^{\circ}$.

Figure 4.- Continued.

(d) $\alpha = 16^{O}$.

Figure 4.- Continued.

(e) α = 20°.

Figure 4.- Concluded.

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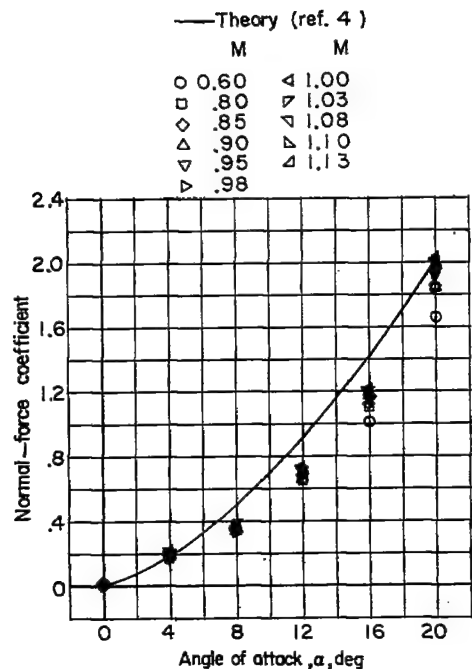
(a) Cylindrical body.

(b) Curved body.

Figure 5.- Comparison of normal-force coefficients. (Flagged symbols
represent data from closed-throat tunnel; unflagged symbols represent
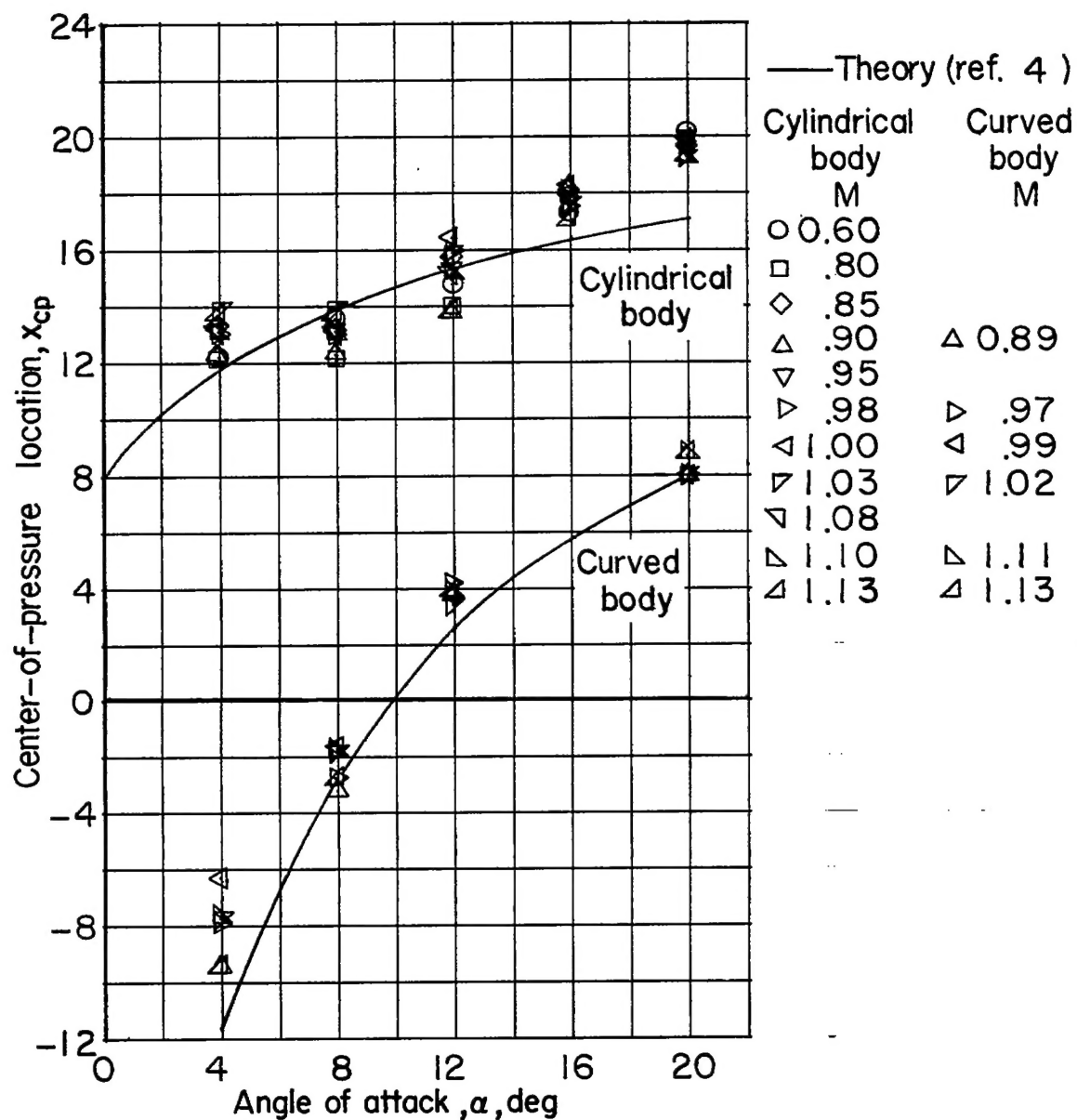data from slotted-throat tunnel.)
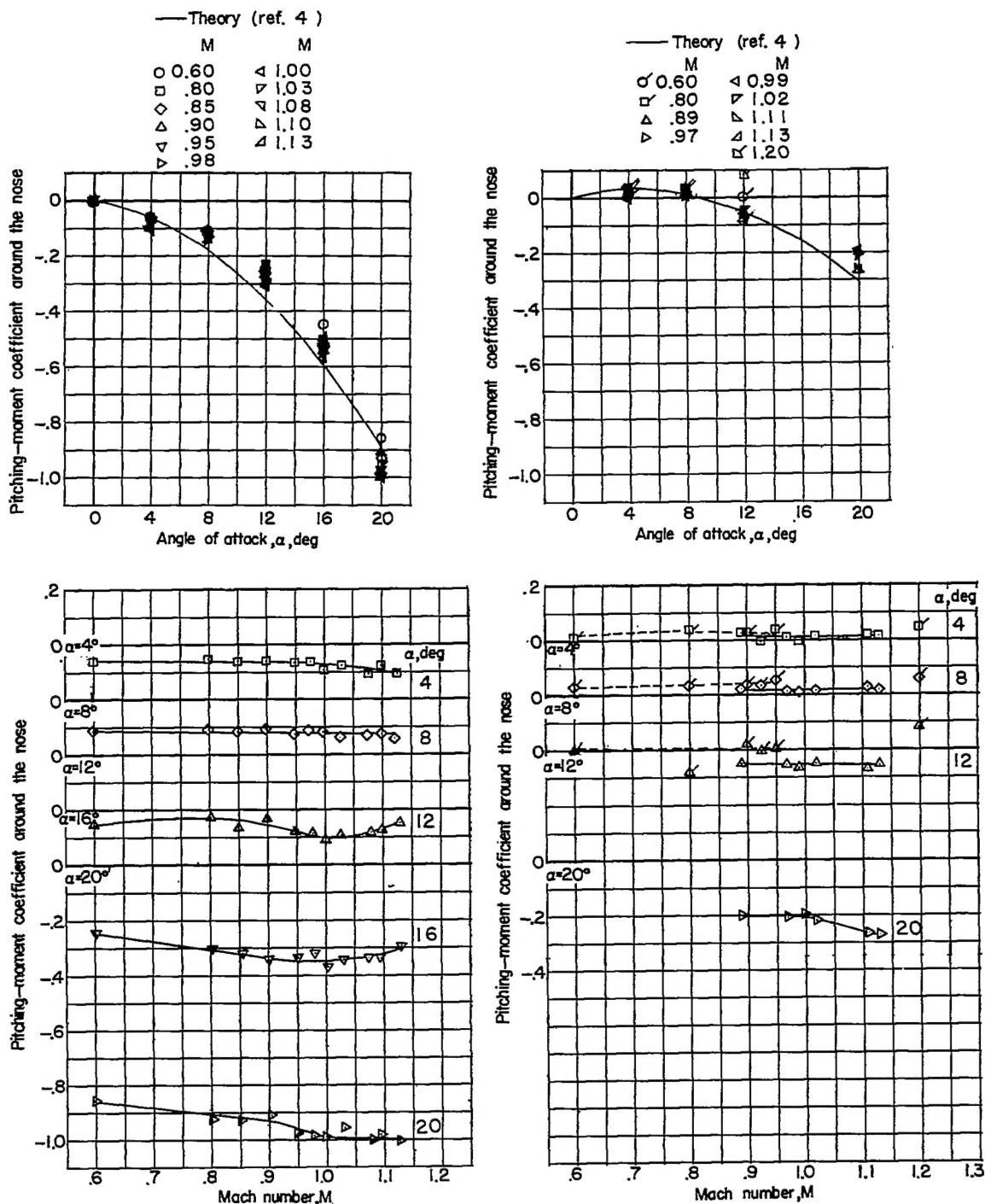
(a) Cylindrical body.

(b) Curved body.

Figure 6.- Comparison of pitching-moment coefficients. (Flagged symbols represent data from closed-throat tunnel; unflagged symbols represent data from slotted-throat tunnel.)

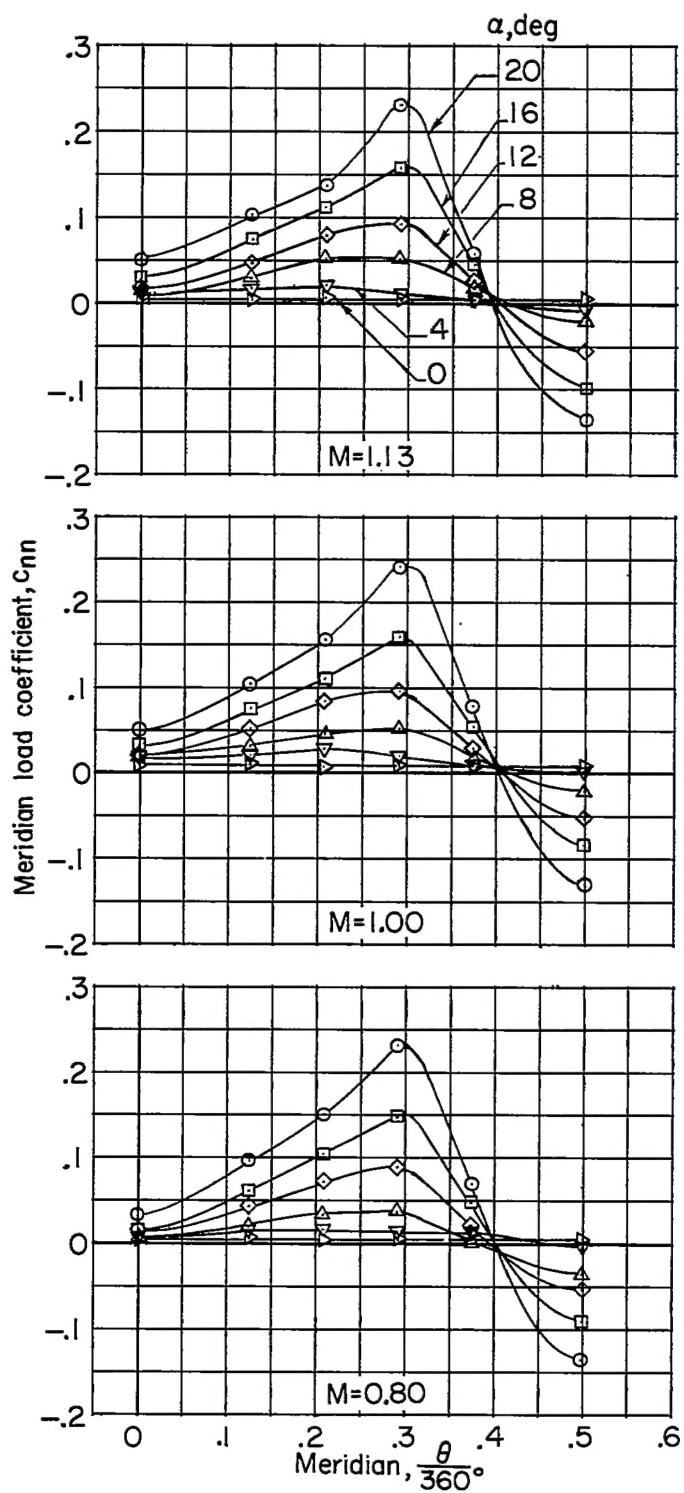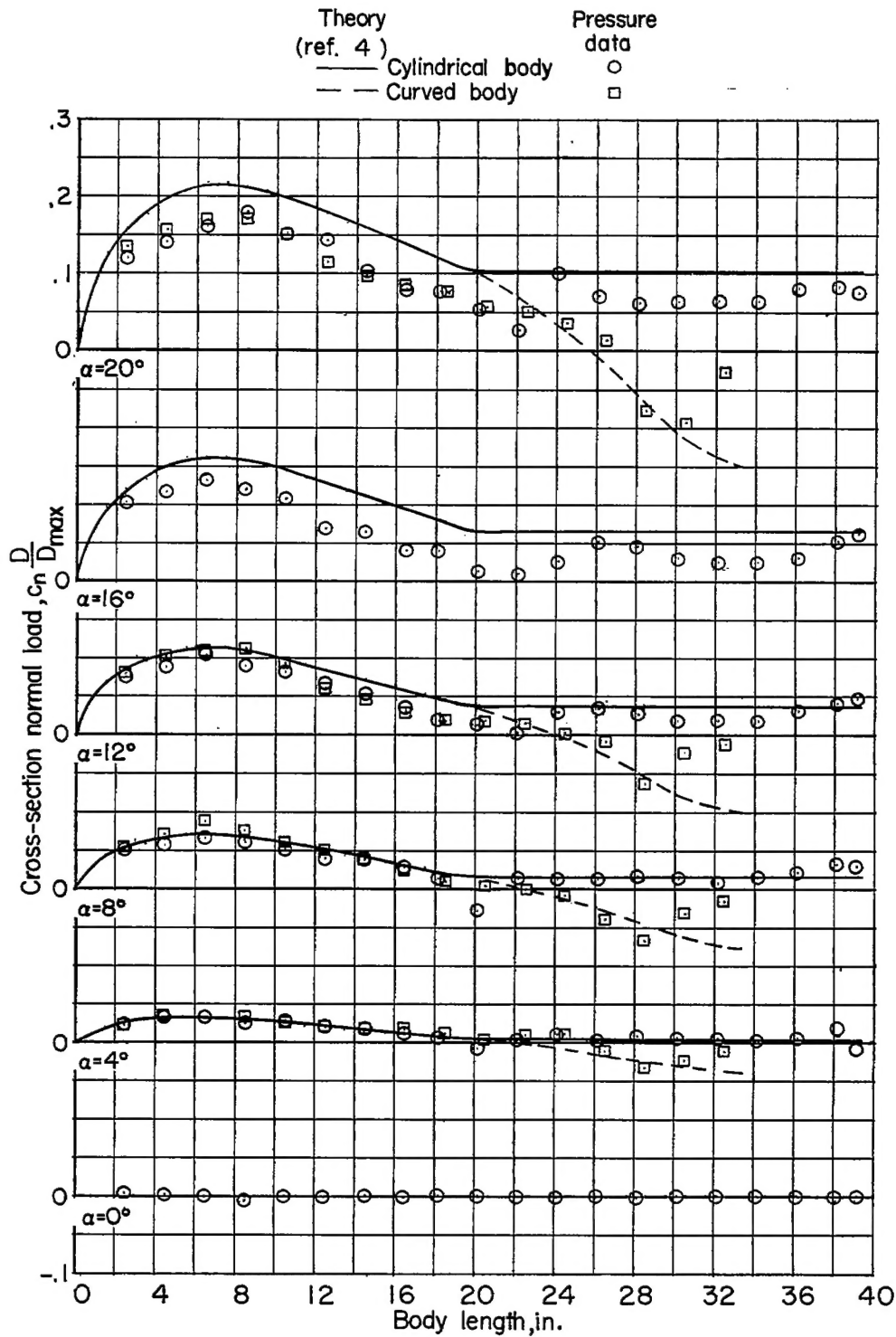Figure 7.- Comparison of center-of-pressure locations.

Figure 8.- Meridian load coefficient. Cylindrical body.

Figure 9.- Comparison of cross-section normal loads.   M = 1.00.